



Geotechnical Subsurface Investigation

Paducah Downtown City Block Development
Paducah, KY

December 20, 2019





December 20, 2019

Ms. Tammara Tracy
Director of Planning
City of Paducah
P.O. Box 2267
300 South 5th Street
Paducah, KY 42002-2267

**Re: Geotechnical Investigation
Paducah Downtown City Block Development**

Dear Ms. Tracy,

The Geotechnical Investigation has been completed for the property located near the intersection of North 2nd Street and Broadway, encompassing the city block parking lot bounded by Jefferson St. to the north, Broadway to the south, Water St. to the east, and North 2nd Street to the west.

We appreciate this opportunity to provide geotechnical services to the City of Paducah Planning Department. Please contact my office if you have questions.

Sincerely,

HDR

A handwritten signature in black ink that reads "Kevin E. Walker".

Kevin E. Walker, PE (AL, GA, NC, PA, TX)
Senior Geotechnical Engineer

A handwritten signature in black ink that reads "Devin Chittenden".

Devin Chittenden, PE
Geotechnical Section Manager

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1 Introduction

This geotechnical report provides a characterization of the subsurface conditions and geotechnical recommendations for use in the design and development of the existing parking lot occupying the city block bounded by Broadway Street, Jefferson Street, North 2nd Street, and Water Street. The conceptual plan for the proposed development includes a four story hotel located along Jefferson Street, and two mixed use three story buildings located along Broadway Street. Borings were advanced and soil samples were collected and delivered to the HDR laboratory for further testing and analysis. Geotechnical parameters and foundation recommendations are provided in this report resulting from the evaluations of soil conditions at the proposed site.

2 Geology

The United States Geological Survey (USGS) 7.5-minute quadrangle map for Paducah East, KY indicates that the Subject Property is located at an elevation of approximately 335 - 340 feet above mean sea level (amsl). The topography in the Subject Property is flat, with a very gentle grade toward the north/northeast away from the south-adjacent Tennessee Valley Divide. Surface runoff drains into stormwater inlets that channelize runoff into the Ohio River.

The Subject Property is situated along the northern edge of the East Gulf Coastal Plain Province, which includes most of the lower Mississippi River / Mid-South Delta region. This portion of the coastal plain is characterized by the Mississippi Embayment, which is a large fluvial floodplain with relatively flat to gently sloping topography that provides drainage pathways over much of the central and eastern portions of North America, including the Ohio River valley. The Embayment was initially formed as a topographic low during the Proterozoic, precipitated by crustal weaknesses that created many structural deformities including the Reelfoot Rift of the New Madrid Seismic Zone. By the end of the Paleozoic, much of the regional basin was infilled with shallow marine deposits, forming the base of the Embayment today as limestone, shale, and sandstones. Regional subsidence and deposition following the Paleozoic resulted in the thick accumulation of Mesozoic and younger unconsolidated strata that generally dip towards the Mississippi River, increasing in thickness to as much as 3,000 feet, with strata becoming progressively younger towards the center of the basin. The local vicinity is considered seismically active from the New Madrid Seismic Zone to the west/southwest and the Wabash Valley Fault System situated northeast of the Subject Property.

Geologically, the Subject Property is immediately underlain with Holocene alluvium consisting of reworked clay, silt, sand, and gravel deposits, which are further underlain by a lower confining layer of Eocene marine deposits. These deposits are often characterized with thinly bedded to laminated dark gray to black elastic silt and light to pale gray micaceous fine sand. Buried artificial fill including cinders, bricks, and metallic fragments are not uncommon in this area along the shores of the Ohio River. Depth to Mississippian carbonate bedrock is anticipated to be approximately 100 to 150 feet below grade near the Subject Property. Surface drainage appears to flow towards the Ohio River to the

north/northeast, and groundwater is expected to generally mirror surface drainage. Depth to groundwater within the Subject Property is generally less than 30 feet, and is highly dependent upon the adjoining Ohio River stage.

3 Subsurface Exploration

In October of 2019 a subsurface investigation was conducted at this site by HDR, utilizing Geotechnology, Inc. as a drilling sub-consultant. The exploration program included a total of fifteen (15) Standard Penetration Test (SPT) borings. Seven (7) borings were advanced at the location of the proposed hotel and four (4) borings were advanced at each of the proposed mixed use buildings. Eleven (11) of the borings were advanced to a depths of 40 feet, three were advanced to 80 feet, and one boring was extended to 100 feet in depth. Each boring was advanced with a CME-55 truck-mounted drill rig using three and one quarter (3 ¼) inch hollow stem augers to penetrate cohesive materials, and switching to mud rotary to penetrate the deeper granular materials. A plan sheet depicting the boring locations is provided in Appendix A. The test boring locations are tabulated below:

Table 3-1. Test Boring Locations

Boring No.	Location	Latitude	Longitude	Surface Elevation	Depth
B-1	Proposed Hotel	37.08871°	88.59595°	335.5 ft.	100 ft.
B-2	Proposed Hotel	37.08863°	88.59591°	334.8 ft.	40 ft.
B-3	Proposed Hotel	37.08912°	88.59494°	334.2 ft.	80 ft.
B-4	Proposed Hotel	37.08904°	88.59484°	334.3 ft.	40 ft.
B-5	Proposed Hotel	37.08876°	88.59571°	336.4 ft.	40 ft.
B-6	Proposed Hotel	37.08885°	88.59548°	336.4 ft.	40 ft.
B-7	Proposed Hotel	37.08898°	88.59517°	335.4 ft.	40 ft.
B-8	Mixed Use Building	37.08801°	88.59526°	337.8 ft.	80 ft.
B-9	Mixed Use Building	37.08805°	88.59549°	337.1 ft.	40 ft.
B-10	Mixed Use Building	37.08818°	88.59508°	336.9 ft.	40 ft.
B-11	Mixed Use Building	37.08813°	88.59507°	336.7 ft.	40 ft.
B-12	Mixed Use Building	37.08823°	88.59497°	336.6 ft.	40 ft.
B-13	Mixed Use Building	37.08821°	88.59488°	336.0 ft.	40 ft.
B-14	Mixed Use Building	37.08842°	88.59450°	336.7 ft.	40 ft.
B-15	Mixed Use Building	37.08833°	88.59445°	336.3 ft.	80 ft.

Standard Penetration Tests (SPT) were obtained at five (5) foot intervals until reaching the plan depths. The SPT N values within the advanced borings ranged from 0 to 100 blows per foot, with an overall averages of 34 blows per foot. Shelby tube sampling was also

performed to obtain undisturbed samples for use in unconfined compression and consolidation testing. Groundwater levels were recorded at the completion of the drilling operations within borings B-4, B-5, and B-14 at depths of 8.6 ft. (EL. 325.7), 20.9 ft. (EL. 315.5), and 26.9 ft. (EL. 309.8), respectively. Auger refusal was not encountered. However, traces of construction debris in the form of brick and concrete fragments were encountered from just below the parking lot subgrade material to a depth of up to 12 feet in borings B-1, B-2, B-3, B-4, B-6, B-7, B-8, and B-12. This debris is described as Fill on the borings. Boring logs from borings B-1 through B-15 are provided in Appendix B.

All soil specimens were delivered to HDR for laboratory testing and further analysis, which included the following tests:

Atterberg Limits	AASHTO T-89 and T-90
Sieve Analysis	ASTM D-1140
Natural Moisture Content	AASHTO T-265
Unconfined Compression (Q_u)	AASHTO T-208
Consolidation	AASHTO T-216
pH Testing	AASHTO T-288
Resistivity	ASTM G-187

The materials near the surface to approximately 25 feet in depth primarily classified silty clay with sand (CL-ML) and lean clay with sand (CL). Samples recovered below approximately 25 feet primarily classified as silty sand (SM), poorly graded gravel with sand (GP), well-graded sand with clay and gravel, (SW-SC), and poorly graded sand with clay and gravel (SP-SM). The full laboratory testing results are located in Appendix C.

Based on the results of both the SPT N values and laboratory classification and strength testing, material properties for the soils encountered were determined and representative soil groups were established. Soil Group No. 1 is representative of the northwestern half of the block along Jefferson Street, and Soil Group No. 2 is representative of the southeastern half along Broadway Street. The following table presents recommended material properties for each soil group.

Table 3-2. Recommended Soil Parameters

Location/ Soil Group	Elev. (ft)	Depth (ft)	ASTM Soil Type	Phi Angle	Unit Weight γ (pcf)	Avg. N Values (bpf)	Total Shear Strength (psf)	Effective Shear Strength (psf)	Soil Strain E_{50}	Soil Modulus k (pci)
Soil Group No. 1 (Boring Nos. 1 through 7)	335.3 - 330.0	0.0 - 5.3	CL (Fill)	26	120	12	1200	240	0.007	500
	330.0 - 325.4	5.3 - 9.9	CL, CL-ML (Residual)	24	120	6	600	120	0.01	100
	325.4 - 318.0	9.9 - 17.3	CL, CL-ML (Residual)	26	120	9	1000	200	0.007	300
	318.0 - 307.6	17.3 - 27.7	CL-ML (Residual)	30	120	20	2000	400	0.005	500
	307.6 - 302.3	27.7 - 33.0	GP (Residual)	32	115	19	0	0	-	60
	302.3 - 292.9	33.0 - 42.4	GP (Residual)	38	130	41	0	0	-	125

Table 3-2. Recommended Soil Parameters

Location/ Soil Group	Elev. (ft)	Depth (ft)	ASTM Soil Type	Phi Angle	Unit Weight γ (pcf)	Avg. N Values (bpf)	Total Shear Strength (psf)	Effective Shear Strength (psf)	Soil Strain E_{50}	Soil Modulus k (pci)
	292.9 - 278.3	42.4 - 57.0	GP, SM (Residual)	28	115	6	0	0	-	20
	278.3 - 235.3	57.0 - 100.0	SM (Residual)	38	130	93	0	0	-	125
Soil Group No. 2 (Borings Nos. 8 through 15)	336.8 - 329.8	0.0 - 7.0	CL, CH (Fill)	26	120	15	1200	240	0.007	500
	329.8 - 313.8	7.0 - 23.0	CL, CH (Residual)	26	120	12	1000	200	0.007	300
	313.8 - 308.1	23.0 - 28.7	SP-SC (Residual)	32	115	21	0	0	-	60
	308.1 - 294.4	28.7 - 42.4	SW-SC, SP-SC (Residual)	38	130	65	0	0	-	125
	294.4 - 273.8	42.4 - 63.0	SM (Residual)	28	115	9	0	0	-	20
	273.8 - 236.8	63.0 - 100.0	SM (Residual)	38	130	75	0	0	-	125

In addition to laboratory classifications and strength testing, pH and resistivity tests were also conducted to determine the corrosiveness of the materials encountered. The purpose of corrosion and deterioration testing is to provide soils data for use by a structural engineer to provide any necessary protection to the piling, concrete, reinforcing steel, etc. Corrosion and deterioration protection requirements and guidelines for piling are set forth in LRFD Section 10.7.5. The corrosion and deterioration testing results are summarized in Table 3-3 below and are included in Appendix C.

Table 3-3. Corrosion and Deterioration Test Summary

Boring No.	Sample Depth	pH	Resistivity (ohm·cm)
B-1	9.0 ft. to 20.5 ft.	7.3	2,720
B-3	14.0 ft. to 25.5 ft.	3.9	5,200
B-8	28.3 ft. to 39.8 ft.	5.9	7,600
B-10	24.0 ft. to 35.5 ft.	6.1	8,400

The following soil conditions should be considered as indicative of a potential pile corrosion or deterioration situation:

- Resistivity less than 2,000 ohm-cm
- pH less than 5.5
- pH between 5.5 and 8.5 in soils with high organic content

- Sulfate concentrations greater than 1,000 ppm

The following soil conditions should be considered as indicative of a potential steel reinforcement corrosion or deterioration situation:

- Resistivity less than 3,000 ohm-cm
- Sulfate concentrations greater than 200 ppm
- Chloride concentrations greater than 100 ppm
- The chloride and sulfate testing is waived if the resistivity is greater than or equal to 5000 ohm-cm

Results of the corrosion and deterioration testing indicated that the site has a marginal potential for pile or steel reinforcement deterioration based on the resistivity values and the geographical location of the project site. Interpretation of the data and corrosion protection of the foundation structural components should be discussed with the structural engineer for the project.

4 Seismic Considerations

Due to its relative proximity to the New Madrid Seismic Zone (NMSZ), McCracken County is considered vulnerable to severe ground shaking. The following spectral response acceleration coefficients were obtained from Section 1613 of the 2018 Kentucky Building Code, Second Edition, dated April 2019. Values for S_s (0.2-second spectral acceleration, 2% probability of exceedance in 50 years) and S_1 (1.0 second spectral acceleration, 2% probability of exceedance in 50 years) were obtained through the 2008 US Geological Survey National Seismic Mapping Project database and adjusted for the 2015 International Building Code.

Table 4-1. Seismic Acceleration Parameters

Spectral Response Acceleration Coefficients				
County	S_s	$S_{s,0}$	S_1	$S_{1,0}$
McCracken	2.124	1.068	0.759	0.366

The project site classifies as Site Class D based on the average SPT values obtained to a depth of 100 feet. An acceleration coefficient for this project site was obtained from Applied Technology Council (ATC) Seismic Hazards web site, which utilizes ASCE7-16 methodology. The ATC website resulted a site-modified peak ground acceleration ($PGAM$) of 0.669 with a 2% probability of exceedance in 50 years.

Preliminary analyses of the subsurface conditions in the SPT borings were performed to evaluate the likelihood of liquefaction during an extreme seismic event. The screening, identification, and evaluation of the geotechnical seismic hazards at the project site were completed using analyses conducted in accordance with Idriss and Boulanger Soil Liquefaction during Earthquakes (2008). Based on the results of the seismic hazard evaluation, it is believed the soils are susceptible to shear strength loss during the seismic event. A detailed seismic design was not included in the scope of this report. We understand that deep foundations are likely to be considered for the proposed hotel and

the mixed use buildings. If so, further analysis and discussion with the structural engineer will be required to determine the liquefaction intervals and how those intervals will affect the seismic design of the foundations including the estimated downdrag loads. The additional downdrag loads can be included in the foundations or ground mitigation options could be evaluated.

4.1 Shallow Foundations

The minimum footing embedment should be 24 inches in order to protect against frost penetration. A foundation size of four (4) feet by (60) feet was assumed for the proposed hotel and mixed use buildings. The table below summarizes the allowable bearing capacity for shallow foundations without undercut, with two feet of undercut and with three feet of undercut using granular backfill material (No. 57 Stone or equivalent). Backfill shall extend to a minimum of 1.0 feet outside the foundation footprint. The allowable bearing capacity is based on a factor of safety of 3.0. The results of the bearing capacity analysis are presented below in Table 4-2.

Table 4-2. Bearing Capacity

Bearing Layer Soil Type	Foundation Depth (feet)	Undercut w/Granular Bedding Material (feet)	Allowable Bearing Capacity (psf)
CL	2.0	0.0	1,800
No. 57 Stone / CL	2.0	2.0	2,200
No. 57 Stone / CL	2.0	3.0	2,500

Due to the presences of construction debris encountered at shallow depths throughout the site within the advanced borings, and the unknown conditions which may be exists between the boring locations, shallow foundations are only recommended for supporting lightly loaded structures.

4.1.1 Settlement Analyses

Settlement of the existing foundation soils due to increased vertical stresses directly below the proposed structures must be considered. HDR completed settlement analyses utilizing Settle3D 4.0 to estimate the magnitude and time-rate of settlement which may affect the proposed structures. Settlement parameters were derived from data collected during the subsurface investigation and laboratory testing as well as published correlations.

No foundation loading information for the proposed structures was available at the writing of this report. In order to quantify the potential for settlement, a spread footing foundation size of four (4) by twelve (60) founded 2.0 feet below the ground surface has been assumed. This settlement is based on assumed foundation loads. Settlement analyses should be performed utilizing the actual foundation loading when they become available. Sampled borings indicate the foundation soils to consist of clay with sand and lean clay with sand materials. Consolidation settlement of theses soil layers will occur over time,

and estimated times for 90 percent of the settlement to occur have been calculated. The results of the settlement analyses are presented below in Table 4-3.

Table 4-3. Settlement

Foundation Size	Assumed Foundation Load (psf)	Total Settlement (inches)	Time Rate of Consolidation, $U_{av} = 90\%$ (days)
4'x60'	1,000	0.72	222
4'x60'	1,250	0.82	390
4'x60'	1,500	0.91	405
4'x60'	2,000	1.06	438

4.2 Deep Foundations

Deep foundations may be an alternative to shallow foundations and/or be necessary to achieve the required bearing capacities at this site. A number of different deep foundation types could be utilized and analyzed upon request. The likely most cost effective deep foundation for site subsurface conditions is driven piles or auger cast piles.

Allowable capacity curves have been developed for HP12x53 steel piles, 12 inch steel pipe piles, 14 inch steel pipe piles and 12 inch auger cast pile sections. Both open ended and plugged pipe piles were analyzed. The axial pile analysis for driven piles was performed using the computer program APILE Plus v2018 with a factor of safety of 2.75. The auger cast pile sections were performed using Ensoft Shaft v2017 with a factor of safety of 2.5. The allowable pile capacity curves and the tabular results for the analyses are provided in Appendix D. It should be noted that the Kentucky Building Code limits deep foundation allowable pile capacities to 40 tons per foundation element. Greater allowable capacities may be achieved by performing load testing and/or pile dynamic analyzer testing, which permit lower factors of safety.

Center to center pile spacing should not be less than three (3) times the effective pile diameter.

Lateral analyses requires horizontal loading information, which was not available at the time of this report. Therefore, lateral analyses were not performed on the pile foundation alternatives presented.

5 Recommendations for Construction

5.1 Construction Monitoring

The existing nearby underground utilities and buildings should be monitored during construction of the foundations. If the monitoring program demonstrates that the new construction is adversely impacting the adjacent utilities and buildings, then it may be

necessary for the contractor to adjust the construction methods as needed to prevent damage.

Earthmoving operations and soil compaction will likely require aeration of soils to reduce moisture contents. These activities are generally not practical in wet winter and early spring months for this geographic area. In addition, all foundation and sub-grade soils must be protected against unnecessary manipulation under construction equipment which could work them into an unstable condition. A working surface over approved sub-grade for structures is recommended to have a minimum thickness of 4 inches.

Traces of construction debris were encountered during this investigation. Buried structures, miscellaneous fill materials, old utility trenches, unstable soils and other objectionable subsurface features not encountered in the borings may be present at the site. Construction should be monitored carefully to prevent the use of unstable soils within the proposed structure foundations. Foundation excavation should be inspected by a qualified geotechnical engineer or their representative prior to placing concrete to verify design bearing capacity, and to prevent seating foundations on unstable materials. Any unstable material encountered during construction excavation should be undercut to stable soils and replaced with No. 57 Stone or approved equivalent.

Groundwater was encountered during the drilling operations. Season variations in the water table should be anticipated. Foundation excavations may require dewatering and/or temporary shoring in accordance with OSHA requirements during construction.

Compaction of backfill materials should achieve 95% of maximum dry density at optimum moisture content $\pm 2\%$ in accordance with ASTM D 698 or AASHTO T 99, standard proctor. Representative samples of the all backfill materials shall be tested to establish the compaction requirements. Compaction shall be verified with field density tests performed by qualified soil technicians. The same compaction effort is required for pavement sub-grade soils if applicable for a depth of 8 inches.

Final earth grading should be sloped away from the proposed structures and backfilling of foundations should be compacted to the minimum requirements set forth in the specifications. In addition, the frost depth at the project site is 2.0 feet. All foundations shall be founded a minimum of 2.0 feet below finished grade.

The placement of a vapor barrier under the slabs on grade is recommended.

5.2 Excavations and Backfill Materials

During construction, the excavation for foundations should not be left open to allow the accumulation of water. Foundations should be concreted and backfilled as soon as possible after excavation is complete. If this cannot be done, a 6 inch thick slab of lean concrete shall be placed to protect the foundation supporting materials.

Any material brought from off-site borrow areas should be approved prior to delivery at the site, and shall be clean and free of any contaminated and hazardous materials. In general, acceptable materials include crushed rock, well-graded sand and gravel, and lean clay exhibiting a liquid limit of less than 45 percent and a plasticity index of less than 20 percent. Satisfactory soil materials for structural fill are defined as those complying with ASTM D

2487 soil classification groups GW, GM, SM, SW, and CL and may include GP, GC, SP, and SC soils. Soil fill should not include any rocks larger than 4 inches in diameter or any significant amount of organics or debris. Any rocks in a cohesive fill should be completely contained within a soil matrix.

Excavation must be performed in accordance with all applicable federal, state, and local standards, including OSHA 29CFR Part 1926 – Excavations and its appendices. Fill soils are to be considered Type C soil. This document states that excavation safety is the responsibility of the contractor. Reference to this OSHA requirement should be included in the project specification. Slope heights, slope inclinations and/or excavation depths should in no case exceed those specified in local, state, or federal safety regulations, including current OSHA excavation and trench safety standards. According to OSHA regulations, side slopes and/or bracing must be designed by a professional engineer for any excavations extending to a depth greater than 20 feet. Where variable fill and/or groundwater is present, flatter slopes than those required by OSHA could be required to maintain the stability of the excavations(s). It should be noted that the subsurface soil types may vary beyond the boring location.

5.3 Control Surface Water

The control of surface runoff will be necessary to prevent erosion of exposed soils, especially on slopes, and the softening of exposed subgrades in excavations. Surficial drainage of slopes, ditches, trench drains, and pumping from sumps should be used as needed to readily remove any surface water, where needed. A drainage plan to collect and control the flow of surface runoff around the construction area should be carefully thought out and implemented before site grading begins. Throughout the duration of construction, the drainage plan should be periodically reviewed and modified as needed.

6 Limitations to Report

The soil descriptions and indicated boundaries discussed and depicted in this report are based on engineering interpretation of available subsurface information obtained at selected locations and may not necessarily reflect the actual variations in subsurface conditions between borings and samples.

Should such variations become apparent during construction, it will be necessary to re-evaluate the subsurface profile based upon on-site observations of the conditions.

7 References



Kentucky Building Code, 2018; Department of Housing, Buildings, and Construction, Frankfort, Kentucky

Applied Technology Council (ATC); Seismic Hazards. Online. Accessed December 13, 2019.

Boulanger, R.W., et al (2008); Soil Liquefaction during Earthquakes; Earthquake Engineering Research Institute.

Appendix A: Boring Layout

LEGEND

-  BORING SAMPLE LOCATION
-  ENVIRONMENTAL BORING SAMPLE LOCATION

DATA SOURCE: ESRI

0 Feet 100

BING MAPS HYBRID



Appendix B: Boring Logs



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 2

State <u>Kentucky</u>	Latitude <u>37.08871⁰</u>	Longitude <u>-88.59595⁰</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>335.5 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/5/2019</u> Completed <u>11/5/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-1</u> Total Depth <u>100 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 335.5 ft					
		CONCRETE					
		FILL					
		Medium stiff, brown, lean CLAY with sand	SS-1	1.5	1.2	5-4-3	SPT
5		Soft to stiff, brown, silty CLAY with sand	SS-2	3.0 4.0	0.8	0-2-2	SPT
			SS-3	5.5 6.5	1.4	0-2-4	SPT
10			SS-4	8.0 9.0 10.5	1.5	2-6-7	SPT
		RESIDUAL SOIL AT 12.5'					
15			SS-5	14.0 15.5	1.2	1-2-3	SPT
20			SS-6	19.0 20.5	1.5	3-5-7	SPT
25		Loose to very dense, brown and gray, poorly graded GRAVEL with sand	SS-7	22.3 24.0 25.5	1.2	15-17-18	SPT
30			SS-8	29.0 30.5	1.5	2-3-4	SPT
35			SS-9	33.5 35.0	0.5	10-13-14	SPT
40			SS-10	38.5 40.0	0.1	1-3-8	SPT
45			SS-11	43.5 45.4	0.9	50-50/0.4	SPT
50			SS-12	48.5 50.0	0.3	6-5-7	SPT
55		Loose to very dense, gray and brown, silty SAND	SS-13	51.8 53.5 55.0	1.5	2-3-4	SPT
60			SS-14	58.5	1.5	8-28-21	SPT



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 2 of 2

State <u>Kentucky</u>	Latitude <u>37.08871⁰</u>	Longitude <u>-88.59595⁰</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>335.5 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/5/2019</u> Completed <u>11/5/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-1</u> Total Depth <u>100 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type	
Depth	Symbol	Rock Core	Core No.	Run	Rec (ft.)	Rec. (%)	RQD (%)	
60		<i>Continued from previous page</i>						
		Elev. = 275.5 ft			60.0			
65			SS-15		63.5 64.4	0.9	50-50/0.4	SPT
70			SS-16		68.5 69.4	0.9	27-50/0.4	SPT
75			SS-17		73.5 74.4	0.9	48-50/0.4	SPT
80								
85			SS-18		83.5 85.0	1.5	16-31-41	SPT
90			SS-19		88.5 89.4	0.8	27-50/0.4	SPT
95			SS-20		93.5 94.8	1.3	39-41-50/0.3	SPT
100			SS-21		98.5 100.0	1.5	7-8-18	SPT
		Boring Terminated at 100.0 ft. (Elev. 235.5)						
105		NOTES Boring offset from original location						
110								
115								
120								



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 1

State <u>Kentucky</u>	Latitude <u>37.08863^o</u>	Longitude <u>-88.59591^o</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>334.8 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/4/2019</u> Completed <u>11/4/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-2</u> Total Depth <u>40.5 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 334.8 ft					
		CONCRETE					
		FILL					
		Soft to stiff, red and brown, lean CLAY with sand	SS-1	1.5	0.3	6-2-5	SPT
5			SS-2	3.0 4.0	1.1	1-1-3	SPT
		RESIDUAL SOIL					
		Very soft to stiff, gray and brown, silty CLAY with sand	SS-3	5.5 6.5	1.2	0-0-0	SPT
10			SS-4	8.0 9.0 10.5	1.2	0-1-4	SPT
15			SS-5	14.0 15.5	1.5	2-4-5	SPT
20			SS-6	19.0 20.5	1.5	3-4-4	SPT
25			SS-7	24.0 25.5	1.5	2-3-4	SPT
30			SS-8	29.0 30.5	1.5	1-3-6	SPT
35		Medium dense to dense, brown, poorly graded GRAVEL with sand	SS-9	34.0 35.5	0.7	18-15-12	SPT
40		Boring Terminated at 40.5 ft. (Elev. 294.3)	SS-10	39.0 40.5	1.0	29-23-17	SPT
45							
50							
55							
60							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 2

State <u>Kentucky</u>	Latitude <u>37.08912⁰</u>	Longitude <u>-88.59494⁰</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>334.2 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/6/2019</u> Completed <u>11/6/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-3</u> Total Depth <u>80 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 334.2 ft					
		CONCRETE					
		FILL Very stiff to hard, gray, lean CLAY with sand	SS-1	1.5		19-10-7	SPT
5			SS-2	3.0			
				4.0		1-4-12	SPT
			SS-3	5.5			
				6.5		5-4-46	SPT
10			SS-4	8.0			
				9.0		1-2-3	SPT
				10.0			
		RESIDUAL SOIL Medium stiff to hard, brown, dark brown and gray, silty CLAY with sand					
15			SS-5	14.0		6-8-11	SPT
				15.5			
20			SS-6	19.0		7-12-22	SPT
				20.5			
25			SS-7	24.0		6-11-14	SPT
				25.5			
				27.3			
30		Very loose to dense, brown, poorly graded GRAVEL with sand	SS-8	29.0		1-0-0	SPT
				30.5			
35			SS-9	33.5		8-16-31	SPT
				35.0			
40			SS-10	38.5		3-5-27	SPT
				40.0			
45			SS-11	43.5		2-0-2	SPT
				45.0			
50			SS-12	48.5		9-0-0	SPT
				50.0			
55			SS-13	53.5		5-4-7	SPT
				55.0			
				57.5			
60		Very dense, light gray and brown, silty SAND	SS-14	58.5		8-32-	SPT



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 2 of 2

State <u>Kentucky</u>	Latitude <u>37.08912^o</u>	Longitude <u>-88.59494^o</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>334.2 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/6/2019</u> Completed <u>11/6/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-3</u> Total Depth <u>80 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Rock Core	Core No.	Run	Rec (ft.)	Rec. (%)	RQD (%)
60		<i>Continued from previous page</i>					
		Elev. = 274.2 ft		59.9		50/0.4	
65			SS-15	63.5 64.4		30-50/0.4	SPT
70			SS-16	68.5 69.3		50-50/0.3	SPT
75			SS-17	73.5 74.4		38-50/0.4	SPT
80			SS-18	78.5 79.4		32-50/0.4	SPT
		Boring Terminated at 80.0 ft. (Elev. 254.2)					
85	<p><u>NOTES</u> Boring offset from original location</p> <p>Split spoons at 3.0', 8.0' and 55.0' resulted in no recovery</p>						
90							
95							
100							
105							
110							
115							
120							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 1

State <u>Kentucky</u>	Latitude <u>37.08904⁰</u>	Longitude <u>-88.59484⁰</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>334.3 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>10/28/2019</u> Completed <u>10/28/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-4</u> Total Depth <u>40 ft.</u>	Depth to Water <u>8.6 ft.</u> Date Measured <u>10/29/2019</u>	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 334.3 ft					
		CONCRETE					
		FILL					
		Medium stiff, brown, lean CLAY with sand	SS-1	1.5	1.0	1-2-4	SPT
5				3.0			
				4.0			
				6.0	0.4	1-3-3	SPT
		Soft to medium stiff, black and brown, lean CLAY with sand	SS-2	6.5	0.2	1-3-2	SPT
				8.0			
				8.5			
10				10.0	0.5	1-2-1	SPT
				12.3			
		RESIDUAL SOIL					
		Very stiff to hard, brown, silty CLAY with sand					
15			SS-5	14.0	1.5	3-8-11	SPT
				15.5			
20			SS-6	19.0	1.3	4-10-18	SPT
				20.5			
25			SS-7	24.0	1.4	7-15-20	SPT
				25.5			
				27.3			
		Dense to very dense, brown, poorly graded GRAVEL with sand					
30			SS-8	29.0	1.5	2-9-21	SPT
				30.5			
35			SS-9	33.5	0.8	15-29-40	SPT
				35.0			
40			SS-10	38.5	0.5	15-22-14	SPT
				40.0			
		Boring Terminated at 40.0 ft. (Elev. 294.3)					
45		NOTES No PID readings identified					
50		Collected sample No. CBPSB04010406 at 1345 on 10/28/2019 from 4.0'-6.0'.					
55		Collected sample No. CBPSB04012830 at 1448 on 10/28/2019 from 28.0'-30.0'.					
60							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 2

State <u>Kentucky</u>	Latitude <u>37.08876°</u>	Longitude <u>-88.59571°</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>336.4 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>10/29/2019</u> Completed <u>11/4/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-5</u> Total Depth <u>39.9 ft.</u>	Depth to Water <u>20.9 ft.</u> Date Measured <u>11/4/2019</u>	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 336.4 ft					
		CONCRETE					
		RESIDUAL SOIL					
		Stiff, brown, lean CLAY with sand	SS-1	1.5	0.0	8-9-5	SPT
5				3.0			
			SS-2	4.0	0.1	12-8-4	SPT
				5.5			
		Soft to very stiff, brown, silty CLAY with sand	SS-3	6.5	1.2	1-1-2	SPT
10				8.0			
			SS-4	9.0	1.5	2-4-6	SPT
				10.5			
15				14.0			
			SS-5	15.5	1.5	3-3-4	SPT
20				19.0			
			SS-6	20.5	1.5	4-7-9	SPT
25				24.0			
			SS-7	25.5	0.9	7-5-4	SPT
30				27.3			
		Medium dense to very dense, brown and dark brown, poorly graded GRAVEL with sand	SS-8	29.0	1.1	4-13-15	SPT
				30.5			
35				33.5			
			SS-9	35.0	1.5	25-36-41	SPT
40				38.5			
			SS-10	39.9	1.1	19-32-50/0.4	SPT
		Boring Terminated at 39.9 ft. (Elev. 296.5)					
45		NOTES					
		Split spoon at 1.5' resulted in no recovery					
50		No PID readings identified					
		Metals composite 1.5'-7.0'					
55		Collected sample No. CBPSB05010608 at 1505 on 10/29/2019 from 6.0'-8.0'.					
60		Collected sample No. CBPSB05012225 at 1029 on					



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 2 of 2

State <u>Kentucky</u>	Latitude <u>37.08876^o</u>	Longitude <u>-88.59571^o</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>336.4 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>10/29/2019</u> Completed <u>11/4/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-5</u> Total Depth <u>39.9 ft.</u>	Depth to Water <u>20.9 ft.</u> Date Measured <u>11/4/2019</u>	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Core No.	Run	Rec (ft.)	Rec. (%)	RQD (%)
60		<i>Continued from previous page</i>					
		Elev. = 276.4 ft					
		10/29/2019 from 22.0'-25.0'.					
65		Collected sample No. CBPSB0501GW at 0730 on 10/30/2019.					
70							
75							
80							
85							
90							
95							
100							
105							
110							
115							
120							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 1

State <u>Kentucky</u>	Latitude <u>37.08898^o</u>	Longitude <u>-88.59517^o</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>335.4 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>10/29/2019</u> Completed <u>10/29/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-7</u> Total Depth <u>40 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 335.4 ft					
	CONCRETE						
	FILL						
		Very soft to medium stiff, gray and brown, lean CLAY with sand	SS-1	1.5	0.4	2-2-3	SPT
5			SS-2	3.0 4.0	0.3	3-1-3	SPT
			SS-3	5.5 6.5 7.0	0.0	2-1-1	SPT
	RESIDUAL SOIL						
		Medium stiff to very stiff, brown, silty CLAY with sand	SS-4	9.0 10.5	0.3	50-10-4	SPT
15			SS-5	14.0 15.5	1.4	1-3-5	SPT
20			SS-6	19.0 20.5	1.2	3-6-10	SPT
25			SS-7	24.0 25.5	1.4	4-8-14	SPT
	GRAVEL						
		Loose to very dense, brown, poorly graded GRAVEL with sand	SS-8	29.0 30.5	0.9	11-21-43	SPT
35			SS-9	33.5 35.0	0.7	11-26-15	SPT
40			SS-10	38.5 40.0	0.9	3-4-5	SPT
		Boring Terminated at 40.0 ft. (Elev. 295.4)					
45		NOTES Split spoon at 6.5' resulted in no recovery					
50							
55							
60							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 2

State <u>Kentucky</u>	Latitude <u>37.08801⁰</u>	Longitude <u>-88.59526⁰</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>337.8 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/14/2019</u> Completed <u>11/15/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-8</u> Total Depth <u>79.2 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i>					
		Elev. = 337.8 ft					
		CONCRETE					
		FILL					
		Stiff, brown, sandy fat CLAY	SS-1	1.5	1.0	2-3-6	SPT
5		Very stiff, brown and gray, lean CLAY with sand	SS-2	3.0 4.0	0.9	2-11-15	SPT
		RESIDUAL SOIL					
		Stiff to very stiff, brown, lean CLAY with sand	SS-3	5.5 6.5	1.3	4-7-11	SPT
10			SS-4	8.0 9.0 10.5	1.5	2-6-7	SPT
15			SS-5	14.0 15.5	1.5	3-4-8	SPT
20			ST-1	19.0 21.0	1.0	50	ST
25		Medium dense, brown, poorly graded SAND with clay and gravel (and/or silty clay and gravel)	SS-6	24.0 25.5	1.3	7-5-6	SPT
30		Very dense, brown, well-graded SAND with clay and gravel (and/or silty clay and gravel)	SS-7	28.3 29.8	1.2	18-31-47	SPT
35			SS-8	33.3 34.8	0.9	27-26-32	SPT
40			SS-9	38.3 39.8	0.4	9-27-33	SPT
45		Very loose to loose, gray and grayish brown, silty SAND	SS-10	43.3 44.8	0.2	5-4-5	SPT
50			SS-11	48.3 49.8	0.5	1-1-2	SPT
55			SS-12	53.3 54.8	0.4	2-4-4	SPT
60			SS-13	58.3	1.5	2-4-6	SPT



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 2 of 2

State <u>Kentucky</u>	Latitude <u>37.08801⁰</u>	Longitude <u>-88.59526⁰</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>337.8 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/14/2019</u> Completed <u>11/15/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-8</u> Total Depth <u>79.2 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type	
Depth	Symbol	Rock Core	Core No.	Run	Rec (ft.)	Rec. (%)	RQD (%)	
60		<i>Continued from previous page</i>						
		Elev. = 277.8 ft			59.8			
		61.6						
		Dense to very dense, gray, silty SAND						
65		SS-14			63.3 64.8	1.3	21-25-14	SPT
70		SS-15			68.3 69.6	1.3	25-44- 50/0.3	SPT
75		SS-16			73.3 74.6	0.9	19-49- 50/0.3	SPT
80	SS-17	79.2		78.3 79.2	0.3	48-50/0.4	SPT	
	Boring Terminated at 79.2 ft. (Elev. 258.6)							
85	<u>NOTES</u> Boring offset from original location							
90								
95								
100								
105								
110								
115								
120								



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 1

State <u>Kentucky</u>	Latitude <u>37.08805°</u>	Longitude <u>-88.59549°</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>337.1 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/15/2019</u> Completed <u>11/15/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-9</u> Total Depth <u>40.5 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 337.1 ft					
		CONCRETE					
		RESIDUAL SOIL					
		Stiff, brown, gray and black, sandy fat CLAY	SS-1	1.5	1.4	2-5-7	SPT
5			SS-2	3.0 4.0	1.2	2-6-7	SPT
		Medium stiff to hard, brown, lean CLAY with sand	SS-3	5.5 6.5	1.4	2-5-4	SPT
10			SS-4	8.0 9.0 10.5	1.3	1-2-4	SPT
15			SS-5	14.0 15.5	1.5	2-3-5	SPT
20			SS-1	19.0 19.4	0.4	100	ST
25			SS-6	24.0 25.5	1.2	17-29-28	SPT
30			SS-7	29.0 30.5	1.5	26-36-35	SPT
35		Medium dense to very dense, brown, poorly graded SAND with clay and gravel (and/or silty clay and gravel)	SS-8	32.3 34.0 34.9	0.9	26-50/0.4	SPT
40			SS-9	39.0 40.5	1.5	20-12-5	SPT
		Boring Terminated at 40.5 ft. (Elev. 296.6)					
45		NOTES Boring offset from original location					
50							
55							
60							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 1

State <u>Kentucky</u>	Latitude <u>37.08818^o</u>	Longitude <u>-88.59508^o</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>336.9 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/11/2019</u> Completed <u>11/11/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-10</u> Total Depth <u>40.5 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 336.9 ft					
		CONCRETE					
		RESIDUAL SOIL					
		Stiff to very stiff, brown and gray, sandy fat CLAY					
5			SS-1	2.3	0.8	3-13-8	SPT
			SS-2	3.8	1.0	4-10-15	SPT
				5.5			
			SS-3	7.0	1.5	2-3-7	SPT
				8.5			
10		Medium stiff to stiff, brown, lean CLAY with sand	SS-4	9.0	1.1	2-5-7	SPT
				10.5			
15			SS-5	14.0	1.5	1-2-4	SPT
				15.5			
20		Medium dense to very dense, brown, poorly graded SAND with clay and gravel (and/or silty clay and gravel)	ST-1	19.0	2.0	100	ST
				21.0			
25			SS-6	24.0	1.1	1-8-18	SPT
				25.5			
30			SS-7	29.0	1.5	21-36-50	SPT
				30.5			
35		Dense to very dense, brown, well-graded SAND with clay and gravel (and/or silty clay and gravel)	SS-8	34.0	1.2	38-50-42	SPT
				35.5			
40		Boring Terminated at 40.5 ft. (Elev. 296.4)	SS-9	39.0	1.5	5-18-14	SPT
				40.5			
45		NOTES Boring offset from original location					
50							
55							
60							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 2

State <u>Kentucky</u>	Latitude <u>37.08813⁰</u>	Longitude <u>-88.59507⁰</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>336.7 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/13/2019</u> Completed <u>11/13/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>22 ft.</u>	
Hole Number <u>B-11</u> Total Depth <u>40.5 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 336.7 ft					
	▴ ▽ ▾	CONCRETE					
	▨	RESIDUAL SOIL Stiff to hard, brown and gray, sandy fat CLAY	SS-1	1.5 1.8 2.8	0.0		SPT
5	▨		SS-2	4.3	1.3	3-6-8	SPT
	▨		SS-3	5.8 6.2	1.4	2-6-7	SPT
	▨	Medium stiff to stiff, brown, lean CLAY with sand	SS-4	6.5 8.0 9.0	1.4	1-3-4	SPT
10	▨		SS-5	10.5	1.5	1-3-5	SPT
15	▨		SS-6	14.0 15.5	1.5	2-3-5	SPT
20	▨		SS-7	19.0 20.5	1.4	4-4-11	SPT
25	▨	Dense to very dense, brown, poorly graded SAND with clay and gravel (and/or silty clay and gravel)	SS-8	22.3 24.0 25.5	1.2	5-20-21	SPT
30	▨		SS-9	29.0 30.5	1.4	21-40-35	SPT
35	▨	Dense to very dense, brown, well-graded SAND with clay and gravel (and/or silty clay and gravel)	SS-10	32.3 34.0 35.5	1.5	26-38-30	SPT
40	▨		SS-11	39.0 40.5	1.5	8-18-20	SPT
45		Boring Terminate at 40.5 ft. (Elev. 296.2)					
50		NOTES Boring offset from original location Water well located 60 ft. West of B-11 Currently patched with asphalt pavement, notes settlement issues					
55		Collected sample No. CBPSB11010206 at 0830 on 11/13/2019 from 2.0'-6.0'.					
60		Collected sample No. CBPSB11020206 at 0830 on					



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 2 of 2

State <u>Kentucky</u>	Latitude <u>37.08813^o</u>	Longitude <u>-88.59507^o</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>336.7 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/13/2019</u>	Completed <u>11/13/2019</u>
Driller <u>N. Gonzales</u>	Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>22 ft.</u>
Hole Number <u>B-11</u>	Total Depth <u>40.5 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Core No.	Run	Rec (ft.)	Rec. (%)	RQD (%)
60		<i>Continued from previous page</i> Elev. = 276.7 ft					
		11/13/2019 from 2.0'-6.0'.					
65		Collected sample No. CBPSB11012426 at 0920 on 11/13/2019 from 24.0'-26.0'.					
70		Collected sample No. CBPSB1101GW, VOG, SVOG, F/U Metals at 1130 on 11/13/2019.					
75		Collected sample No. CBPSB1102GW, VOG, SVOG at 1130 on 11/13/2019.					
80							
85							
90							
95							
100							
105							
110							
115							
120							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 1

State <u>Kentucky</u>	Latitude <u>37.08823⁰</u>	Longitude <u>-88.59497⁰</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>336.6 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/12/2019</u> Completed <u>11/12/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-12</u> Total Depth <u>40.5 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 336.6 ft					
		CONCRETE					
		FILL					
		Soft to stiff, brown and brownish gray, lean CLAY with sand					
5			SS-1	2.3	0.6	3-6-5	SPT
			SS-2	3.8	0.5	4-2-1	SPT
				4.0			
				5.5			
				6.5			
		RESIDUAL SOIL					
		Medium stiff to stiff, gray and brownish gray, lean CLAY with sand					
10			SS-3	7.4	1.5	2-3-4	SPT
			SS-4	8.0	1.5	1-2-3	SPT
				10.5			
15				14.0	1.5	3-7-7	SPT
				15.5			
				17.3			
		Medium dense to very dense, brown, poorly graded SAND with clay and gravel (and/or silty clay and gravel)					
20			ST-1	19.0	2.0	100	ST
				21.0			
25				24.0	0.7	3-8-17	SPT
				25.5			
30				29.0	1.1	15-24-36	SPT
				30.5			
				32.3			
		Dense to very dense, brown, well-graded SAND with clay and gravel (and/or silty clay and gravel)					
35			SS-8	34.0	0.8	48-50/0.3	SPT
				34.8			
40			SS-9	39.0	0.8	38-22-11	SPT
				40.5			
		Boring Terminated at 40.5 ft. (Elev. 296.1)					
45		NOTES Boring offset from original location					
50							
55							
60							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 1

State <u>Kentucky</u>	Latitude <u>37.08821^o</u>	Longitude <u>-88.59488^o</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>336 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/12/2019</u> Completed <u>11/12/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-13</u> Total Depth <u>40.5 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 336.0 ft					
		CONCRETE					
		RESIDUAL SOIL					
		Stiff to very stiff, brown and brownish gray, lean CLAY with sand	SS-1	2.3	1.0	1-4-6	SPT
5			SS-2	3.8 4.0	1.1	4-8-10	SPT
		Very stiff, brown, gray and brownish gray, sandy fat CLAY					
			SS-3	5.5 6.4	1.0	5-10-15	SPT
10			SS-4	7.3 8.0	1.1	0-10-14	SPT
		Stiff, brown, lean CLAY with sand					
			SS-5	10.5 12.3	1.5	2-5-6	SPT
15							
		Very dense, brown, poorly graded SAND with clay and gravel (and/or silty clay and gravel)	ST-1	14.0 15.5	1.6	80	ST
20							
			SS-6	17.3 19.0	1.5	17-28-25	SPT
25							
			SS-7	21.0 24.0	1.1	13-24-29	SPT
30							
		Dense to very dense, brown, well-graded SAND with clay and gravel (and/or silty clay and gravel)	SS-8	25.5 29.0	1.5	30-43-47	SPT
35							
			SS-9	30.5 32.3	1.5	10-19-21	SPT
40							
		Boring Terminated at 40.5 ft. (Elev. 295.5)					
45		NOTES Boring offset from original location					
50							
55							
60							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 1

State <u>Kentucky</u>	Latitude <u>37.08842^o</u>	Longitude <u>-88.59450^o</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>336.7 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/13/2019</u> Completed <u>11/13/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-14</u> Total Depth <u>40.5 ft.</u>	Depth to Water <u>26.9 ft.</u> Date Measured <u>11/14/2019</u>	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 336.7 ft					
	▽ ▽ ▽	CONCRETE					
	▨	RESIDUAL SOIL Very stiff, brown and gray, sandy fat CLAY	SS-1	1.5	1.2	2-8-10	SPT
5	▨	Stiff to very stiff, brown and gray, lean CLAY with sand	SS-2	3.0 4.0	1.2	3-8-11	SPT
	▨		SS-3	5.5 6.5	1.4	2-5-8	SPT
10	▨		SS-4	8.0 9.0 10.5	1.3	1-5-7	SPT
15	▨		SS-5	14.0 15.5	1.5	2-6-6	SPT
20	▨		SS-6	19.0 20.5	1.4	2-7-11	SPT
25	▨		SS-7	24.0 25.5	1.5	5-8-11	SPT
30	▨		SS-8	29.0 30.5	1.3	13-40-46	SPT
35	▨	Very dense, brown, well-graded SAND with clay and gravel (and/or silty clay and gravel)	SS-9	32.3 34.0 35.4	1.4	43-49-50/0.4	SPT
40	▨		SS-10	39.0 40.5	1.2	46-45-40	SPT
		Boring Terminate at 40.5 ft. (Elev. 296.2)					
45		NOTES Boring offset from original location					
50		Collected sample No. CBPSB14010206 at 1230 on 11/13/2019 from 2.0'-6.0'.					
55		Collected sample No. CBPSB14012830 at 1345 on 11/13/2019 from 28.0'-30.0'.					
		Collected sample No. CBPSB1401GW at 0730 on 11/14/2019.					
60							



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 1 of 2

State <u>Kentucky</u>	Latitude <u>37.08833⁰</u>	Longitude <u>-88.59445⁰</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>336.3 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/13/2019</u> Completed <u>11/14/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-15</u> Total Depth <u>79.5 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type
Depth	Symbol	Description	Rock Core	Run	Rec (ft.)	Rec. (%)	RQD (%)
0		<i>Ground Line</i> Elev. = 336.3 ft					
		RESIDUAL SOIL Medium stiff to stiff, brown, sandy fat CLAY	SS-1	1.5	1.3	2-3-5	SPT
5			SS-2	3.0 4.0	1.5	3-7-8	SPT
			SS-3	5.5 6.5	1.4	2-3-7	SPT
10		Medium stiff to very stiff, brown, lean CLAY with sand	SS-4	8.0 9.0 10.5	1.5	1-3-5	SPT
15			SS-5	14.0 15.5	1.5	2-5-7	SPT
20			ST-1	19.0 21.0	2.0	100	ST
25			SS-6	24.0 25.5	1.4	4-10-12	SPT
30		Medium dense to very dense, brown, poorly graded SAND with clay and gravel (and/or silty clay and gravel)	SS-7	29.0 30.5	1.0	7-13-14	SPT
35			SS-8	33.5 35.0	0.9	28-50-47	SPT
40		Dense to very dense, brown, well-graded SAND with clay and gravel (and/or silty clay and gravel)	SS-9	38.5 40.0	0.6	14-18-21	SPT
45			SS-10	43.5 45.0	0.8	4-33-39	SPT
50		Loose to very dense, gray, silty SAND	SS-11	48.5 50.0	0.8	6-4-5	SPT
55			SS-12	53.5 55.0	0.0	3-4-7	SPT
60			SS-13	58.5	1.5	4-6-10	SPT



SUBSURFACE INVESTIGATION
BORING LOG

Sheet No. 2 of 2

State <u>Kentucky</u>	Latitude <u>37.08833^o</u>	Longitude <u>-88.59445^o</u>
County <u>McCracken</u>	Location _____	
Project Name <u>Paducah City Block Development</u>	Surface Elevation <u>336.3 ft</u>	
Job No. <u>10197216</u>	Dated Started <u>11/13/2019</u> Completed <u>11/14/2019</u>	
Driller <u>N. Gonzales</u> Logged by <u>J. Hilt</u>	Depth to Water: Immediate <u>N/A</u>	
Hole Number <u>B-15</u> Total Depth <u>79.5 ft.</u>	Depth to Water <u>N/A</u> Date Measured _____	

Lithology		Overburden	Sample No.	Depth	Rec. (ft.)	Blows	Type	
Depth	Symbol	Rock Core	Core No.	Run	Rec (ft.)	Rec. (%)	RQD (%)	
60		<i>Continued from previous page</i>						
		Elev. = 276.3 ft			60.0			
65			SS-14		63.5 65.0	1.1	7-12-14	SPT
70			SS-15		68.5 69.5	1.0	49-50/0.5	SPT
75			SS-16		73.5 75.0	1.3	25-24-29	SPT
80			SS-17		78.5 79.5	1.0	21-50/0.5	SPT
			79.5					
		Boring Terminated at 79.5 ft. (Elev. 256.8)						
85		<u>NOTES</u> Split spoon at 53.5' resulted in no recovery						
90								
95								
100								
105								
110								
115								
120								

Appendix C: Laboratory Testing



Project Name : Paducah Downtown Develoment
Location : McCracken County, Kentucky
Job Number : 10197216

Moisture Data
 (AASHTO T255-T265 / ASTM C566-D2216)

Soil No.	Boring No.	Station & Offset	Sample No.	Depth	Description of Soil	pH	Natural Moisture Content (%)
1	B-1		SS-1	1.5	3.0	Brown Lean Clay with Sand	18.6
3			SS-2	6.5	8.0	Brown Silty Clay with Sand	25.5
3			SS-3	6.5	8.0	Brown Silty Clay with Sand	19.2
3			SS-4	9.0	10.5	Brown Silty Clay with Sand	18.7
3			SS-5	14.0	15.5	Brown Silty Clay with Sand	21.7
3			SS-6	19.0	20.5	Brown Silty Clay with Sand	15.5
4			SS-7	24.0	25.5	Brown Poorly Graded Gravel with Sand	17.2
4			SS-8	29.0	30.5	Brown Poorly Graded Gravel with Sand	19.9
4			SS-9	33.5	35.0	Brown Poorly Graded Gravel with Sand	19.5
4			SS-10	38.5	40.0	Brown & Gray Poorly Graded Gravel with Sand	27.5
4			SS-11	43.5	45.0	Brown Poorly Graded Gravel with Sand	14.5
4			SS-12	48.5	50.0	Brown & Gray Poorly Graded Gravel with Sand	35.4
6			SS-13	53.5	55.0	Gray & Brown Silty Sand	31.3
6			SS-14	58.5	60.0	Gray Silty Sand	31.6
6			SS-15	63.5	64.5	Gray Silty Sand	27.5
6			SS-16	68.5	69.5	Gray Silty Sand	39.5
6			SS-17	73.5	74.5	Gray Silty Sand	29.4
6			SS-18	83.5	85.0	Gray Silty Sand	31.4
6			SS-19	88.5	89.5	Gray Silty Sand	32.9
6			SS-20	93.5	95.0	Gray Silty Sand	27.5
6			SS-21	98.5	100.0	Gray Silty Sand	31.4
1	B-2		SS-1	1.5	3.0	Red & Brown Lean Clay with Sand	10.5
1			SS-2	4.0	5.5	Brown Lean Clay with Sand	25.1
3			SS-3	6.5	8.0	Gray Silty Clay with Sand	26.6
3			SS-4	9.0	10.5	Gray Silty Clay with Sand	22.3
3			SS-5	14.0	15.5	Gray Silty Clay with Sand	19.8
3			SS-6	19.0	20.5	Brown Silty Clay with Sand	15.4
3			SS-7	24.0	25.5	Brown Silty Clay with Sand	23.4
3			SS-8	29.0	30.5	Brown Silty Clay with Sand	20.6
4			SS-9	34.0	35.5	Brown Poorly Graded Gravel with Sand	15.2
4			SS-10	39.0	40.5	Brown Poorly Graded Gravel with Sand	17.5
	B-3		SS-1	3.0	4.5	No Sample	
2			SS-2	5.5	7.0	Gray Lean Clay with Sand	22.4
			SS-3	8.0	9.5	No Sample	
3			SS-4	10.5	12.0	Brown Silty Clay with Sand	22.9
3			SS-5	14.0	15.5	Brown, Dark Brown & Gray Silty Clay with Sand	19.5
3			SS-6	19.0	20.5	Brown Silty Clay with Sand	18.6
3			SS-7	24.0	25.5	Brown Silty Clay with Sand	20.0
4			SS-8	29.0	30.5	Brown Poorly Graded Gravel with Sand	23.1
4			SS-9	33.5	35.0	Brown Poorly Graded Gravel with Sand	22.9
4			SS-10	38.5	40.0	Brown Poorly Graded Gravel with Sand	21.5
4			SS-11	43.5	45.0	Brown Poorly Graded Gravel with Sand	18.3
4			SS-12	48.5	50.0	Brown Poorly Graded Gravel with Sand	19.0
			SS-13	55.0	56.5	No Sample	
5			SS-14	58.5	60.0	Light Gray Silty Sand	25.1
5			SS-15	63.5	64.5	Light Gray Silty Sand	21.2
5			SS-16	68.5	69.5	Brown Silty Sand	23.7
5			SS-17	73.5	74.5	Brown Silty Sand	27.7
5			SS-18	78.5	79.5	Brown Silty Sand	27.8
2	B-4		SS-1	1.5	3.0	Brown Lean Clay with Sand	22.0
2			SS-2	4.0	5.5	Brown Lean Clay with Sand	20.9
1			SS-3	6.5	8.0	Black Lean Clay with Sand	26.8
1			SS-4	9.0	10.5	Brown Lean Clay with Sand	25.0
3			SS-5	14.0	15.5	Brown Silty Clay with Sand	19.5
3			SS-6	19.0	20.5	Brown Silty Clay with Sand	16.3

Project Name : Paducah Downtown Develoment
Location : McCracken County, Kentucky
Job Number : 10197216

Moisture Data
(AASHTO T255-T265 / ASTM C566-D2216)

Soil Boring		Station & Offset	Sample		Description of Soil	pH	Natural Moisture Content (%)
No.	No.		No.	Depth			
3			SS-7	24.0	25.5	Brown Silty Clay with Sand	22.1
4			SS-8	29.0	30.5	Brown Poorly Graded Gravel with Sand	19.2
4			SS-9	33.5	35.0	Brown Poorly Graded Gravel with Sand	16.1
4			SS-10	38.5	40.0	Brown Poorly Graded Gravel with Sand	17.9
	B-5		SS-1	1.5	3.0	No Sample	
2			SS-2	4.0	5.5	Brown Lean Clay with Sand	22.4
3			SS-3	6.5	8.0	Brown Silty Clay with Sand	20.1
3			SS-4	9.0	10.5	Brown Silty Clay with Sand	22.1
3			SS-5	14.0	15.5	Brown Silty Clay with Sand	19.2
3			SS-6	19.0	20.5	Brown Silty Clay with Sand	20.2
3			SS-7	24.0	25.5	Brown Silty Clay with Sand	22.7
4			SS-8	29.0	30.5	Brown Poorly Graded Gravel with Sand	16.9
4			SS-9	33.5	35.0	Brown Poorly Graded Gravel with Sand	16.8
4			SS-10	38.5	39.9	Dark Brown Poorly Graded Gravel with Sand	15.0
1	B-6		SS-1	1.5	3.0	Dark Brown Lean Clay with Sand	15.9
1			SS-2	4.0	5.5	Dark Brown Lean Clay with Sand	18.5
1			SS-3	6.5	8.0	Dark Brown Lean Clay with Sand	19.7
1			SS-4	9.0	10.0	Dark Brown Lean Clay with Sand	27.6
3			SS-5	14.0	15.5	Brown Silty Clay with Sand	22.3
3			SS-6	19.0	20.5	Brown Silty Clay with Sand	20.6
3			SS-7	24.0	25.5	Brown Silty Clay with Sand	12.6
4			SS-8	29.0	30.5	Brown Poorly Graded Gravel with Sand	14.9
4			SS-9	34.0	35.5	Brown Poorly Graded Gravel with Sand	33.8
4			SS-10	39.0	40.5	Brown Poorly Graded Gravel with Sand	15.0
1	B-7		SS-1	1.5	3.0	Gray Lean Clay with Sand	13.1
1			SS-2	4.0	5.5	Brown Lean Clay with Sand	24.7
			SS-3	6.5	8.0	No Sample	
3			SS-4	9.0	10.5	Brown Silty Clay with Sand	20.7
3			SS-5	14.0	15.5	Brown Silty Clay with Sand	21.1
3			SS-6	19.0	20.5	Brown Silty Clay with Sand	19.5
3			SS-7	24.0	25.5	Brown Silty Clay with Sand	19.5
4			SS-8	29.0	30.5	Brown Poorly Graded Gravel with Sand	15.5
4			SS-9	33.5	35.0	Brown Poorly Graded Gravel with Sand	17.7
4			SS-10	38.5	40.0	Brown Poorly Graded Gravel with Sand	22.8
8	B-8		SS-1	1.5	3.0	Brown Sandy Fat Clay	24.8
7			SS-2	4.0	5.5	Brown & Gray Lean Clay with Sand	18.0
9			SS-3	6.5	8.0	Brown Lean Clay with Sand	16.8
9			SS-4	9.0	10.5	Brown Lean Clay with Sand	17.3
9			SS-5	14.0	15.5	Brown Lean Clay with Sand	21.6
9			ST-1	19.0	21.0	Brown Lean Clay with Sand	
10			SS-6	24.0	25.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)	20.6
11			SS-7	28.3	29.8	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)	16.5
11			SS-8	33.3	34.8	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)	15.9
11			SS-9	38.3	39.8	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)	25.6
12			SS-10	43.3	44.8	Gray Silty Sand	23.9
12			SS-11	48.3	49.8	Grayish Brown Silty Sand	34.7
12			SS-12	53.3	54.8	Gray Silty Sand	35.3
12			SS-13	58.3	59.8	Gray Silty Sand	43.0
13			SS-14	63.3	64.8	Gray Silty Sand	23.4
13			SS-15	68.3	69.6	Gray Silty Sand	31.1
13			SS-16	73.3	74.6	Gray Silty Sand	28.3
13			SS-17	78.3	79.2	Gray Silty Sand	34.0
8	B-9		SS-1	1.5	3.0	Brown Sandy Fat Clay	24.7
8			SS-2	4.0	5.5	Brown, Gray & Black Sandy Fat Clay	21.6
9			SS-3	6.5	8.0	Brown Lean Clay with Sand	17.7
9			SS-4	9.0	10.5	Brown Lean Clay with Sand	18.1
9			SS-5	14.0	15.5	Brown Lean Clay with Sand	20.3
9			ST-1	19.0	19.4	Brown Lean Clay with Sand	
9			SS-6	24.0	25.5	Brown Lean Clay with Sand	14.6

Project Name : Paducah Downtown Develoment
Location : McCracken County, Kentucky
Job Number : 10197216

Moisture Data
(AASHTO T255-T265 / ASTM C566-D2216)

Soil No.	Boring No.	Station & Offset	Sample		Description of Soil	pH	Natural Moisture Content (%)	
			No.	Depth				
9			SS-7	29.0	30.5	Brown Lean Clay with Sand		13.4
10			SS-8	34.0	34.9	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		16.8
10			SS-9	39.0	40.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		15.8
8	B-10		SS-1	2.3	3.8	Brown Sandy Fat Clay		21.2
8			SS-2	4.0	5.5	Brown & Gray Sandy Fat Clay		19.5
8			SS-3	7.0	8.5	Brown & Gray Sandy Fat Clay		20.1
9			SS-4	9.0	10.5	Brown Lean Clay with Sand		15.3
9			SS-5	14.0	15.5	Brown Lean Clay with Sand		21.1
10			ST-1	19.0	21.0	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		
10			SS-6	24.0	25.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		16.2
10			SS-7	29.0	31.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		15.8
11			SS-8	34.0	35.5	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		17.8
11			SS-9	39.0	39.8	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		14.5
11			SS-9A	39.8	40.5	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		26.4
	B-11		SS-1	1.5	2.8	No Sample		
8			SS-2	2.8	4.3	Brown Sandy Fat Clay		24.7
8			SS-3	4.3	5.8	Brown & Gray Sandy Fat Clay		23.2
9			SS-4	6.5	8.0	Brown Lean Clay with Sand		19.2
9			SS-5	9.0	10.5	Brown Lean Clay with Sand		19.0
9			SS-6	14.0	15.5	Brown Lean Clay with Sand		21.8
9			SS-7	19.0	20.5	Brown Lean Clay with Sand		16.2
10			SS-8	24.0	25.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		19.2
10			SS-9	29.0	30.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		19.1
11			SS-10	34.0	35.5	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		15.9
11			SS-11	39.0	40.5	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		18.4
7	B-12		SS-1	2.3	3.8	Brown Lean Clay with Sand		23.1
7			SS-2	4.0	5.5	Brownish Gray Lean Clay with Sand		40.4
9			SS-3	7.4	8.9	Gray Lean Clay with Sand		20.3
9			SS-4	9.0	10.5	Gray Lean Clay with Sand		20.0
9			SS-5	14.0	15.5	Brownish Gray Lean Clay with Sand		22.2
10			ST-1	19.0	21.0	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		
10			SS-6	24.0	25.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		17.3
10			SS-7	29.0	30.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		16.4
11			SS-8	34.0	34.8	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		14.5
11			SS-9	39.0	40.5	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		17.3
7	B-13		SS-1	2.3	3.8	Brown Lean Clay with Sand		22.8
7			SS-2	4.0	5.5	Brownish Gray Lean Clay with Sand		19.6
8			SS-3	7.3	8.8	Brown & Gray Sandy Fat Clay		20.6
8			SS-4	9.0	10.5	Brownish Gray Sandy Fat Clay		14.5
9			SS-5	14.0	15.5	Brown Lean Clay with Sand		16.6
10			ST-1	19.0	21.0	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		
10			SS-6	24.0	25.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		21.7
10			SS-7	29.0	30.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		16.9
11			SS-8	34.0	35.5	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		17.4
11			SS-9	39.0	40.5	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		25.8
8	B-14		SS-1	1.5	2.3	Brown Sandy Fat Clay		23.8
8			SS-2	4.0	5.5	Brown & Gray Sandy Fat Clay		20.9
9			SS-3	6.5	8.0	Brown & Gray Lean Clay with Sand		17.8
9			SS-4	14.0	15.5	Brown Lean Clay with Sand		21.6
9			SS-5	14.0	15.5	Brown Lean Clay with Sand		18.5
9			SS-6	19.0	20.5	Brown Lean Clay with Sand		19.7
9			SS-7	29.0	30.5	Brown Lean Clay with Sand		14.9
11			SS-8	34.0	35.5	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		16.4
11			SS-9	34.0	35.4	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		15.7
11			SS-10	39.0	40.5	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)		14.7
8	B-15		SS-1	1.5	3.0	Brown Sandy Fat Clay		24.5
8			SS-2	4.0	5.5	Brown Sandy Fat Clay		20.1
8			SS-3	6.5	8.0	Brown Sandy Fat Clay		19.7

Project Name : Paducah Downtown Develoment
 Location : McCracken County, Kentucky
 Job Number : 10197216

Moisture Data
 (AASHTO T255-T265 / ASTM C566-D2216)

Soil Boring		Station & Offset	Sample		Description of Soil	pH	Natural Moisture Content (%)
No.	No.		No.	Depth			
9			SS-4	9.0	10.5	Brown Lean Clay with Sand	18.2
9			SS-5	14.0	15.5	Brown Lean Clay with Sand	20.2
9			ST-1	19.0	21.0	Brown Lean Clay with Sand	
9			SS-6	24.0	25.5	Brown Lean Clay with Sand	17.9
10			SS-7	29.0	30.5	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)	46.8
10			SS-8	33.5	35.0	Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)	13.9
11			SS-9	38.5	40.0	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)	21.2
11			SS-10	43.5	45.0	Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)	13.9
12			SS-11	48.5	50.0	Gray Silty Sand	31.2
			SS-12	53.5	55.0	No Sample	
12			SS-13	58.5	60.0	Gray Silty Sand	32.5
12			SS-14	63.5	65.0	Gray Silty Sand	30.5
12			SS-15	68.5	69.5	Gray Silty Sand	25.1
12			SS-16	73.5	74.6	Gray Silty Sand	30.4
12			SS-16A	74.6	75.0	Gray Silty Sand	29.8
12			SS-17	78.5	78.7	Gray Silty Sand	34.4
12			SS-17A	78.7	79.5	Gray Silty Sand	24.1



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Brown Lean Clay with Sand

Sample No. : SS-4
 Sample Loc. : Boring No. B-4
 Sample Depth : 9.0' to 10.5'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing
4	in.	101.6	mm	
3.5	in.	88.9	mm	
3	in.	76.2	mm	
2.5	in.	63.5	mm	
2	in.	50.8	mm	
1 3/4	in.	45	mm	
1 1/2	in.	38.1	mm	
1 1/4	in.	31.5	mm	
1	in.	25	mm	
3/4	in.	19	mm	
1/2	in.	12.5	mm	
3/8	in.	9.5	mm	100.0
1/4		6.3	mm	
No.4		4.75	mm	98.7
No.6		3.35	mm	
No.10		2	mm	98.1

				% Passing
No.16		1.18	mm	
No.30		0.6	mm	
No.40		0.425	mm	94.3
No.50		0.3	mm	
No.60		0.25	mm	
No.80		0.18	mm	
No.100		0.15	mm	
No.200		0.075	mm	77.6
No.270		0.053	mm	
Hyd. Rd. # 1			mm	
Hyd. Rd. # 2			mm	
Hyd. Rd. # 3			mm	
Hyd. Rd. # 4			mm	
Hyd. Rd. # 5			mm	
Hyd. Rd. # 6			mm	
Hyd. Rd. # 7			mm	

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 0.007 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 25.0
 Liquid Limit (AASHTO T89) : 33
 Plastic Limit (AASHTO T90) : 21
 Plasticity Index : 12
 Liquidity Index : 0.36

AASHTO Composition of Total Sample: M145
 Gravel (3in. + No.10) : 1.9
 Coarse Sand (-No.10 + No.40) : 3.8
 Fine Sand (-No.40 + No.200) : 16.7
 Silt + Clay (-No.200) : 77.6

Activity : NA
 Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-6 (8)
 ASTM Classification: D2487 : CL

ASTM Composition of Total Sample: D2487
 Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 1.3
 Coarse Sand (-No.4 + No.10) : 0.6
 Medium Sand (-No.10 + No.40) : 3.8
 Fine Sand (-No.40 + No.200) : 16.7
 Silt + Clay (-No.200) : 77.6

Approved By : Kevin E. Walker

Soil No. 1



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Brown Lean Clay with Sand

Sample No. : SS-1
 Sample Loc. : Boring No. B-4
 Sample Depth : 1.5' to 3.0'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing
4	in.	101.6	mm	
3.5	in.	88.9	mm	
3	in.	76.2	mm	
2.5	in.	63.5	mm	
2	in.	50.8	mm	
1 3/4	in.	45	mm	
1 1/2	in.	38.1	mm	
1 1/4	in.	31.5	mm	
1	in.	25	mm	
3/4	in.	19	mm	
1/2	in.	12.5	mm	
3/8	in.	9.5	mm	100.0
1/4		6.3	mm	
No.4		4.75	mm	99.4
No.6		3.35	mm	
No.10		2	mm	97.6

				% Passing
No.16		1.18	mm	
No.30		0.6	mm	
No.40		0.425	mm	90.4
No.50		0.3	mm	
No.60		0.25	mm	
No.80		0.18	mm	
No.100		0.15	mm	
No.200		0.075	mm	72.7
No.270		0.053	mm	
Hyd. Rd. # 1			mm	
Hyd. Rd. # 2			mm	
Hyd. Rd. # 3			mm	
Hyd. Rd. # 4			mm	
Hyd. Rd. # 5			mm	
Hyd. Rd. # 6			mm	
Hyd. Rd. # 7			mm	

AASHTO T88

**Method B used for #200 Wash with a soaking time of 1440 minutes*

D50 = 0.009 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 22.0
 Liquid Limit (AASHTO T89) : 32
 Plastic Limit (AASHTO T90) : 21
 Plasticity Index : 11
 Liquidity Index : 0.06

AASHTO Composition of Total Sample: M145
 Gravel (3in. + No.10) : 2.4
 Coarse Sand (-No.10 + No.40) : 7.2
 Fine Sand (-No.40 + No.200) : 17.7
 Silt + Clay (-No.200) : 72.7

Activity : NA
 Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-6 (7)
 ASTM Classification: D2487 : CL

ASTM Composition of Total Sample: D2487
 Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 0.6
 Coarse Sand (-No.4 + No.10) : 1.8
 Medium Sand (-No.10 + No.40) : 7.2
 Fine Sand (-No.40 + No.200) : 17.7
 Silt + Clay (-No.200) : 72.7

Approved By : Kevin E. Walker

Soil No. 2



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Brown Silty Clay with Sand

Sample No. : SS-5
 Sample Loc. : Boring No. B-5
 Sample Depth : 14.0' to 15.5'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing
4	in.	101.6	mm	
3.5	in.	88.9	mm	
3	in.	76.2	mm	
2.5	in.	63.5	mm	
2	in.	50.8	mm	
1 3/4	in.	45	mm	
1 1/2	in.	38.1	mm	
1 1/4	in.	31.5	mm	
1	in.	25	mm	
3/4	in.	19	mm	
1/2	in.	12.5	mm	
3/8	in.	9.5	mm	100.0
1/4		6.3	mm	
No.4		4.75	mm	99.5
No.6		3.35	mm	
No.10		2	mm	99.4

				% Passing
No.16		1.18	mm	
No.30		0.6	mm	
No.40		0.425	mm	97.7
No.50		0.3	mm	
No.60		0.25	mm	
No.80		0.18	mm	
No.100		0.15	mm	
No.200		0.075	mm	79.1
No.270		0.053	mm	
Hyd. Rd. # 1			mm	
Hyd. Rd. # 2			mm	
Hyd. Rd. # 3			mm	
Hyd. Rd. # 4			mm	
Hyd. Rd. # 5			mm	
Hyd. Rd. # 6			mm	
Hyd. Rd. # 7			mm	

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 0.007 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 19.2
 Liquid Limit (AASHTO T89) : 20
 Plastic Limit (AASHTO T90) : 14
 Plasticity Index : 6
 Liquidity Index : 0.84

AASHTO Composition of Total Sample: M145
 Gravel (3in. + No.10) : 0.6
 Coarse Sand (-No.10 + No.40) : 1.7
 Fine Sand (-No.40 + No.200) : 18.6
 Silt + Clay (-No.200) : 79.1

Activity : NA
 Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-4 (2)
 ASTM Classification: D2487 : CL-ML

ASTM Composition of Total Sample: D2487
 Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 0.5
 Coarse Sand (-No.4 + No.10) : 0.1
 Medium Sand (-No.10 + No.40) : 1.7
 Fine Sand (-No.40 + No.200) : 18.6
 Silt + Clay (-No.200) : 79.1

Approved By : Kevin E. Walker

Soil No. 3



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Brown Poorly Graded Gravel with Sand

Sample No. : SS-10
 Sample Loc. : Boring No. B-2
 Sample Depth : 39.0' to 40.5'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing	
4	in.	101.6	mm		
3.5	in.	88.9	mm		
3	in.	76.2	mm		
2.5	in.	63.5	mm		
2	in.	50.8	mm		
1 3/4	in.	45	mm		
1 1/2	in.	38.1	mm		
1 1/4	in.	31.5	mm		
1	in.	25	mm	100.0	
3/4	in.	19	mm	85.5	
1/2	in.	12.5	mm		
3/8	in.	9.5	mm	49.4	
1/4		6.3	mm		
No.4		4.75	mm	26.7	
No.6		3.35	mm		
No.10		2	mm	18.8	

				% Passing	
No.16		1.18	mm		
No.30		0.6	mm		
No.40		0.425	mm	14.1	
No.50		0.3	mm		
No.60		0.25	mm		
No.80		0.18	mm		
No.100		0.15	mm		
No.200		0.075	mm	2.4	
No.270		0.053	mm		
Hyd. Rd. # 1			mm		
Hyd. Rd. # 2			mm		
Hyd. Rd. # 3			mm		
Hyd. Rd. # 4			mm		
Hyd. Rd. # 5			mm		
Hyd. Rd. # 6			mm		
Hyd. Rd. # 7			mm		

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 9.61 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 17.5
 Liquid Limit (AASHTO T89) : NP
 Plastic Limit (AASHTO T90) : NP
 Plasticity Index : NP
 Liquidity Index : NA
 Activity : NA

AASHTO Composition of Total Sample: M145
 Gravel (3in. + No.10) : 81.2
 Coarse Sand (-No.10 + No.40) : 4.7
 Fine Sand (-No.40 + No.200) : 11.7
 Silt + Clay (-No.200) : 2.4

Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-1-a (0)
 ASTM Classification: D2487 : GP

ASTM Composition of Total Sample: D2487
 Coarse Gravel (3in. + 3/4in.) : 14.5
 Fine Gravel (-3/4in. + No.4) : 58.8
 Coarse Sand (-No.4 + No.10) : 7.9
 Medium Sand (-No.10 + No.40) : 4.7
 Fine Sand (-No.40 + No.200) : 11.7
 Silt + Clay (-No.200) : 2.4

Approved By : Kevin E. Walker

Soil No. 4



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Light Gray Silty Sand

Sample No. : SS-15
 Sample Loc. : Boring No. B-3
 Sample Depth : 63.5' to 64.5'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing
4	in.	101.6	mm	
3.5	in.	88.9	mm	
3	in.	76.2	mm	
2.5	in.	63.5	mm	
2	in.	50.8	mm	
1 3/4	in.	45	mm	
1 1/2	in.	38.1	mm	
1 1/4	in.	31.5	mm	
1	in.	25	mm	
3/4	in.	19	mm	
1/2	in.	12.5	mm	
3/8	in.	9.5	mm	
1/4		6.3	mm	
No.4		4.75	mm	100.0
No.6		3.35	mm	
No.10		2	mm	100.0

				% Passing
No.16		1.18	mm	
No.30		0.6	mm	
No.40		0.425	mm	77.7
No.50		0.3	mm	
No.60		0.25	mm	
No.80		0.18	mm	
No.100		0.15	mm	
No.200		0.075	mm	18.6
No.270		0.053	mm	
Hyd. Rd. # 1			mm	
Hyd. Rd. # 2			mm	
Hyd. Rd. # 3			mm	
Hyd. Rd. # 4			mm	
Hyd. Rd. # 5			mm	
Hyd. Rd. # 6			mm	
Hyd. Rd. # 7			mm	

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 0.188 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 21.2
 Liquid Limit (AASHTO T89) : NP
 Plastic Limit (AASHTO T90) : NP
 Plasticity Index : NP
 Liquidity Index : NA

AASHTO Composition of Total Sample: M145

Gravel (3in. + No.10) : 0.0
 Coarse Sand (-No.10 + No.40) : 22.3
 Fine Sand (-No.40 + No.200) : 59.1
 Silt + Clay (-No.200) : 18.6

Activity : NA
 Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-2-4 (0)
 ASTM Classification: D2487 : SM

ASTM Composition of Total Sample: D2487

Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 0.0
 Coarse Sand (-No.4 + No.10) : 0.0
 Medium Sand (-No.10 + No.40) : 22.3
 Fine Sand (-No.40 + No.200) : 59.1
 Silt + Clay (-No.200) : 18.6

Approved By : Kevin E. Walker

Soil No. 5



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Gray Silty Sand

Sample No. : SS-17
 Sample Loc. : Boring No. B-1
 Sample Depth : 73.5' to 74.5'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing
4	in.	101.6	mm	
3.5	in.	88.9	mm	
3	in.	76.2	mm	
2.5	in.	63.5	mm	
2	in.	50.8	mm	
1 3/4	in.	45	mm	
1 1/2	in.	38.1	mm	
1 1/4	in.	31.5	mm	
1	in.	25	mm	
3/4	in.	19	mm	
1/2	in.	12.5	mm	
3/8	in.	9.5	mm	100.0
1/4		6.3	mm	
No.4		4.75	mm	99.6
No.6		3.35	mm	
No.10		2	mm	99.4

				% Passing
No.16		1.18	mm	
No.30		0.6	mm	
No.40		0.425	mm	88.8
No.50		0.3	mm	
No.60		0.25	mm	
No.80		0.18	mm	
No.100		0.15	mm	
No.200		0.075	mm	29.1
No.270		0.053	mm	
Hyd. Rd. # 1			mm	
Hyd. Rd. # 2			mm	
Hyd. Rd. # 3			mm	
Hyd. Rd. # 4			mm	
Hyd. Rd. # 5			mm	
Hyd. Rd. # 6			mm	
Hyd. Rd. # 7			mm	

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 0.138 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 29.4
 Liquid Limit (AASHTO T89) : NP
 Plastic Limit (AASHTO T90) : NP
 Plasticity Index : NP
 Liquidity Index : NA

AASHTO Composition of Total Sample: M145

Gravel (3in. + No.10) : 0.6
 Coarse Sand (-No.10 + No.40) : 10.6
 Fine Sand (-No.40 + No.200) : 59.7
 Silt + Clay (-No.200) : 29.1

Activity : NA
 Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-2-4 (0)
 ASTM Classification: D2487 : SM

ASTM Composition of Total Sample: D2487

Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 0.4
 Coarse Sand (-No.4 + No.10) : 0.2
 Medium Sand (-No.10 + No.40) : 10.6
 Fine Sand (-No.40 + No.200) : 59.7
 Silt + Clay (-No.200) : 29.1

Approved By : Kevin E. Walker

Soil No. 6



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Brownish Gray Lean Clay with Sand

Sample No. : SS-2
 Sample Loc. : Boring No. B-13
 Sample Depth : 4.0' to 5.5'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing	
4	in.	101.6	mm		
3.5	in.	88.9	mm		
3	in.	76.2	mm		
2.5	in.	63.5	mm		
2	in.	50.8	mm		
1 3/4	in.	45	mm		
1 1/2	in.	38.1	mm		
1 1/4	in.	31.5	mm		
1	in.	25	mm		
3/4	in.	19	mm		
1/2	in.	12.5	mm		
3/8	in.	9.5	mm		100.0
1/4		6.3	mm		
No.4		4.75	mm		99.9
No.6		3.35	mm		
No.10		2	mm		99.1

				% Passing	
No.16		1.18	mm		
No.30		0.6	mm		
No.40		0.425	mm		88.6
No.50		0.3	mm		
No.60		0.25	mm		
No.80		0.18	mm		
No.100		0.15	mm		
No.200		0.075	mm		72.5
No.270		0.053	mm		
Hyd. Rd. # 1			mm		
Hyd. Rd. # 2			mm		
Hyd. Rd. # 3			mm		
Hyd. Rd. # 4			mm		
Hyd. Rd. # 5			mm		
Hyd. Rd. # 6			mm		
Hyd. Rd. # 7			mm		

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 0.01 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 19.6
 Liquid Limit (AASHTO T89) : 34
 Plastic Limit (AASHTO T90) : 20
 Plasticity Index : 14
 Liquidity Index : -0.03
 Activity : NA
 Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-6 (9)
 ASTM Classification: D2487 : CL

AASHTO Composition of Total Sample: M145

Gravel (3in. + No.10) : 0.9
 Coarse Sand (-No.10 + No.40) : 10.5
 Fine Sand (-No.40 + No.200) : 16.1
 Silt + Clay (-No.200) : 72.5

ASTM Composition of Total Sample: D2487

Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 0.1
 Coarse Sand (-No.4 + No.10) : 0.8
 Medium Sand (-No.10 + No.40) : 10.5
 Fine Sand (-No.40 + No.200) : 16.1
 Silt + Clay (-No.200) : 72.5

Approved By : Kevin E. Walker

Soil No. 7



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Brown Sandy Fat Clay

Sample No. : SS-1
 Sample Loc. : Boring No. B-14
 Sample Depth : 1.5' to 2.3'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing	
4	in.	101.6	mm		
3.5	in.	88.9	mm		
3	in.	76.2	mm		
2.5	in.	63.5	mm		
2	in.	50.8	mm		
1 3/4	in.	45	mm		
1 1/2	in.	38.1	mm		
1 1/4	in.	31.5	mm		
1	in.	25	mm		
3/4	in.	19	mm		
1/2	in.	12.5	mm		
3/8	in.	9.5	mm		100.0
1/4		6.3	mm		
No.4		4.75	mm		99.4
No.6		3.35	mm		
No.10		2	mm		94.6

				% Passing	
No.16		1.18	mm		
No.30		0.6	mm		
No.40		0.425	mm		62.2
No.50		0.3	mm		
No.60		0.25	mm		
No.80		0.18	mm		
No.100		0.15	mm		
No.200		0.075	mm		52.6
No.270		0.053	mm		
Hyd. Rd. # 1			mm		
Hyd. Rd. # 2			mm		
Hyd. Rd. # 3			mm		
Hyd. Rd. # 4			mm		
Hyd. Rd. # 5			mm		
Hyd. Rd. # 6			mm		
Hyd. Rd. # 7			mm		

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 0.054 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 23.8
 Liquid Limit (AASHTO T89) : 51
 Plastic Limit (AASHTO T90) : 28
 Plasticity Index : 23
 Liquidity Index : -0.16

AASHTO Composition of Total Sample: M145
 Gravel (3in. + No.10) : 5.4
 Coarse Sand (-No.10 + No.40) : 32.4
 Fine Sand (-No.40 + No.200) : 9.6
 Silt + Clay (-No.200) : 52.6

Activity : NA
 Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-7-6 (9)
 ASTM Classification: D2487 : CH

ASTM Composition of Total Sample: D2487

Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 0.6
 Coarse Sand (-No.4 + No.10) : 4.8
 Medium Sand (-No.10 + No.40) : 32.4
 Fine Sand (-No.40 + No.200) : 9.6
 Silt + Clay (-No.200) : 52.6

Approved By : Kevin E. Walker

Soil No. 8



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Brown Lean Clay with Sand

Sample No. : SS-4
 Sample Loc. : Boring No. B-11
 Sample Depth : 6.5' to 8.0'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing
4	in.	101.6	mm	
3.5	in.	88.9	mm	
3	in.	76.2	mm	
2.5	in.	63.5	mm	
2	in.	50.8	mm	
1 3/4	in.	45	mm	
1 1/2	in.	38.1	mm	
1 1/4	in.	31.5	mm	
1	in.	25	mm	
3/4	in.	19	mm	
1/2	in.	12.5	mm	
3/8	in.	9.5	mm	
1/4		6.3	mm	
No.4		4.75	mm	100.0
No.6		3.35	mm	
No.10		2	mm	100.0

				% Passing
No.16		1.18	mm	
No.30		0.6	mm	
No.40		0.425	mm	98.5
No.50		0.3	mm	
No.60		0.25	mm	
No.80		0.18	mm	
No.100		0.15	mm	
No.200		0.075	mm	81.9
No.270		0.053	mm	
Hyd. Rd. # 1			mm	
Hyd. Rd. # 2			mm	
Hyd. Rd. # 3			mm	
Hyd. Rd. # 4			mm	
Hyd. Rd. # 5			mm	
Hyd. Rd. # 6			mm	
Hyd. Rd. # 7			mm	

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 0.006 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 19.2
 Liquid Limit (AASHTO T89) : 29
 Plastic Limit (AASHTO T90) : 18
 Plasticity Index : 11
 Liquidity Index : 0.09

AASHTO Composition of Total Sample: M145
 Gravel (3in. + No.10) : 0.0
 Coarse Sand (-No.10 + No.40) : 1.5
 Fine Sand (-No.40 + No.200) : 16.6
 Silt + Clay (-No.200) : 81.9

Activity : NA
 Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-6 (8)
 ASTM Classification: D2487 : CL

ASTM Composition of Total Sample: D2487
 Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 0.0
 Coarse Sand (-No.4 + No.10) : 0.0
 Medium Sand (-No.10 + No.40) : 1.5
 Fine Sand (-No.40 + No.200) : 16.6
 Silt + Clay (-No.200) : 81.9

Approved By : Kevin E. Walker

Soil No. 9



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Brown Poorly Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)

Sample No. : SS-6
 Sample Loc. : Boring No. B-13
 Sample Depth : 24.0' to 25.5'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing
4	in.	101.6	mm	
3.5	in.	88.9	mm	
3	in.	76.2	mm	
2.5	in.	63.5	mm	
2	in.	50.8	mm	
1 3/4	in.	45	mm	
1 1/2	in.	38.1	mm	
1 1/4	in.	31.5	mm	
1	in.	25	mm	100.0
3/4	in.	19	mm	88.0
1/2	in.	12.5	mm	
3/8	in.	9.5	mm	78.6
1/4		6.3	mm	
No.4		4.75	mm	66.4
No.6		3.35	mm	
No.10		2	mm	54.2

				% Passing
No.16		1.18	mm	
No.30		0.6	mm	
No.40		0.425	mm	31.4
No.50		0.3	mm	
No.60		0.25	mm	
No.80		0.18	mm	
No.100		0.15	mm	
No.200		0.075	mm	10.5
No.270		0.053	mm	
Hyd. Rd. # 1			mm	
Hyd. Rd. # 2			mm	
Hyd. Rd. # 3			mm	
Hyd. Rd. # 4			mm	
Hyd. Rd. # 5			mm	
Hyd. Rd. # 6			mm	
Hyd. Rd. # 7			mm	

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 1.504 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 21.7
 Liquid Limit (AASHTO T89) : 25
 Plastic Limit (AASHTO T90) : 16
 Plasticity Index : 9
 Liquidity Index : 0.68

AASHTO Composition of Total Sample: M145
 Gravel (3in. + No.10) : 45.8
 Coarse Sand (-No.10 + No.40) : 22.8
 Fine Sand (-No.40 + No.200) : 20.9
 Silt + Clay (-No.200) : 10.5

Activity : NA
 Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-2-4 (0)
 ASTM Classification: D2487 : SP-SC

ASTM Composition of Total Sample: D2487

Coarse Gravel (3in. + 3/4in.) : 12.0
 Fine Gravel (-3/4in. + No.4) : 21.6
 Coarse Sand (-No.4 + No.10) : 12.2
 Medium Sand (-No.10 + No.40) : 22.8
 Fine Sand (-No.40 + No.200) : 20.9
 Silt + Clay (-No.200) : 10.5

Approved By : Kevin E. Walker

Soil No. 10



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Brown Well-Graded Sand with Clay and Gravel (and/or Silty Clay and Gravel)

Sample No. : SS-8
 Sample Loc. : Boring No. B-12
 Sample Depth : 34.0' to 34.8'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing	
4	in.	101.6	mm		
3.5	in.	88.9	mm		
3	in.	76.2	mm		
2.5	in.	63.5	mm		
2	in.	50.8	mm		
1 3/4	in.	45	mm		
1 1/2	in.	38.1	mm		
1 1/4	in.	31.5	mm		
1	in.	25	mm		
3/4	in.	19	mm		100.0
1/2	in.	12.5	mm		
3/8	in.	9.5	mm		89.8
1/4		6.3	mm		
No.4		4.75	mm		69.2
No.6		3.35	mm		
No.10		2	mm		46.3

				% Passing	
No.16		1.18	mm		
No.30		0.6	mm		
No.40		0.425	mm		16.1
No.50		0.3	mm		
No.60		0.25	mm		
No.80		0.18	mm		
No.100		0.15	mm		
No.200		0.075	mm		5.5
No.270		0.053	mm		
Hyd. Rd. # 1			mm		
Hyd. Rd. # 2			mm		
Hyd. Rd. # 3			mm		
Hyd. Rd. # 4			mm		
Hyd. Rd. # 5			mm		
Hyd. Rd. # 6			mm		
Hyd. Rd. # 7			mm		

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 2.3 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 14.5
 Liquid Limit (AASHTO T89) : 24
 Plastic Limit (AASHTO T90) : 17
 Plasticity Index : 7
 Liquidity Index : -0.42

AASHTO Composition of Total Sample: M145
 Gravel (3in. + No.10) : 53.7
 Coarse Sand (-No.10 + No.40) : 30.2
 Fine Sand (-No.40 + No.200) : 10.6
 Silt + Clay (-No.200) : 5.5

Activity : NA
 Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-2-4 (0)
 ASTM Classification: D2487 : SW-SC

ASTM Composition of Total Sample: D2487
 Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 30.8
 Coarse Sand (-No.4 + No.10) : 22.9
 Medium Sand (-No.10 + No.40) : 30.2
 Fine Sand (-No.40 + No.200) : 10.6
 Silt + Clay (-No.200) : 5.5

Approved By : Kevin E. Walker

Soil No. 11



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Gray Silty Sand

Sample No. : SS-16
 Sample Loc. : Boring No. B-15
 Sample Depth : 73.5' to 74.6'
 Date Tested : 11/18/19
 Date Reported : 11/22/19

AASHTO T27 :

				% Passing
4	in.	101.6	mm	
3.5	in.	88.9	mm	
3	in.	76.2	mm	
2.5	in.	63.5	mm	
2	in.	50.8	mm	
1 3/4	in.	45	mm	
1 1/2	in.	38.1	mm	
1 1/4	in.	31.5	mm	
1	in.	25	mm	
3/4	in.	19	mm	
1/2	in.	12.5	mm	
3/8	in.	9.5	mm	
1/4		6.3	mm	
No.4		4.75	mm	100.0
No.6		3.35	mm	
No.10		2	mm	100.0

				% Passing
No.16		1.18	mm	
No.30		0.6	mm	
No.40		0.425	mm	97.2
No.50		0.3	mm	
No.60		0.25	mm	
No.80		0.18	mm	
No.100		0.15	mm	
No.200		0.075	mm	27.4
No.270		0.053	mm	
Hyd. Rd. # 1			mm	
Hyd. Rd. # 2			mm	
Hyd. Rd. # 3			mm	
Hyd. Rd. # 4			mm	
Hyd. Rd. # 5			mm	
Hyd. Rd. # 6			mm	
Hyd. Rd. # 7			mm	

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 0.132 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 30.4
 Liquid Limit (AASHTO T89) : NP
 Plastic Limit (AASHTO T90) : NP
 Plasticity Index : NP
 Liquidity Index : NA
 Activity : NA

AASHTO Composition of Total Sample: M145
 Gravel (3in. + No.10) : 0.0
 Coarse Sand (-No.10 + No.40) : 2.8
 Fine Sand (-No.40 + No.200) : 69.8
 Silt + Clay (-No.200) : 27.4

Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-2-4 (0)
 ASTM Classification: D2487 : SM

ASTM Composition of Total Sample: D2487
 Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 0.0
 Coarse Sand (-No.4 + No.10) : 0.0
 Medium Sand (-No.10 + No.40) : 2.8
 Fine Sand (-No.40 + No.200) : 69.8
 Silt + Clay (-No.200) : 27.4

Approved By : Kevin E. Walker

Soil No. 12



SOIL CLASSIFICATION

Project Name : Paducah City Block Development
 Project No. : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory No. : 10197216
 Submitted By : HDR
 Soil Type : Gray Silty Sand

Sample No. : SS-15
 Sample Loc. : Boring No. B-8
 Sample Depth : 68.3' to 69.6'
 Date Tested : 11/21/19
 Date Reported : 12/04/19

AASHTO T27 :

				% Passing
4	in.	101.6	mm	
3.5	in.	88.9	mm	
3	in.	76.2	mm	
2.5	in.	63.5	mm	
2	in.	50.8	mm	
1 3/4	in.	45	mm	
1 1/2	in.	38.1	mm	
1 1/4	in.	31.5	mm	
1	in.	25	mm	
3/4	in.	19	mm	
1/2	in.	12.5	mm	
3/8	in.	9.5	mm	
1/4		6.3	mm	
No.4		4.75	mm	100.0
No.6		3.35	mm	
No.10		2	mm	100.0

				% Passing
No.16		1.18	mm	
No.30		0.6	mm	
No.40		0.425	mm	99.9
No.50		0.3	mm	
No.60		0.25	mm	
No.80		0.18	mm	
No.100		0.15	mm	
No.200		0.075	mm	35.2
No.270		0.053	mm	
Hyd. Rd. # 1			mm	
Hyd. Rd. # 2			mm	
Hyd. Rd. # 3			mm	
Hyd. Rd. # 4			mm	
Hyd. Rd. # 5			mm	
Hyd. Rd. # 6			mm	
Hyd. Rd. # 7			mm	

AASHTO T88

*Method B used for #200 Wash with a soaking time of 1440 minutes

D50 = 0.112 mm

CBR : NA
 Dry Dens. : NA
 Opt. Moist. : NA

Natural Moisture (%) (AASHTO T265) : 31.1
 Liquid Limit (AASHTO T89) : NP
 Plastic Limit (AASHTO T90) : NP
 Plasticity Index : NP
 Liquidity Index : NA
 Activity : NA

AASHTO Composition of Total Sample: M145
 Gravel (3in. + No.10) : 0.0
 Coarse Sand (-No.10 + No.40) : 0.1
 Fine Sand (-No.40 + No.200) : 64.7
 Silt + Clay (-No.200) : 35.2

Sp. Gr. (AASHTO T100) : NA
 AASHTO Classification: M145 : A-4 (0)
 ASTM Classification: D2487 : SM

ASTM Composition of Total Sample: D2487
 Coarse Gravel (3in. + 3/4in.) : 0.0
 Fine Gravel (-3/4in. + No.4) : 0.0
 Coarse Sand (-No.4 + No.10) : 0.0
 Medium Sand (-No.10 + No.40) : 0.1
 Fine Sand (-No.40 + No.200) : 64.7
 Silt + Clay (-No.200) : 35.2

Approved By : Kevin E. Walker

Soil No. 13



UNCONFINED COMPRESSION TEST

AASHTO: T-208

Page 1 of 2

Project Name : Paducah Downtown Development	Sample # : ST-1
Project # : 10197216	Sample Loc. : Boring No. B-15
Project County : McCracken	Sample Depth : 19.5' to 20.0'
Project State : Kentucky	Date Tested : 11/20/2019
Laboratory # : 10197216	Date Reported : 11/21/2019
Submitted By : HDR	

Soil Type : Garth	Initial Height : 5.80 in
Wet Density : 130.4 pcf	Initial Diameter : 2.86 in
Dry Density : 110.6 pcf	Proving Ring : #22734
Moisture : 17.8 %	

RESULTS:	Axial Load	Corrected Area	Unit Strain	Stress
#	lbs	sf	%	Ksf
1	0.0	0.04	0.0	0.00
2	3.0	0.04	0.3	0.07
3	9.0	0.04	0.5	0.20
4	19.0	0.04	0.8	0.42
5	30.1	0.05	1.0	0.67
6	40.1	0.05	1.3	0.89
7	47.9	0.05	1.6	1.06
8	52.0	0.05	1.8	1.15
9	59.8	0.05	2.1	1.31
10	52.0	0.05	2.4	1.41
11	77.1	0.05	2.8	1.68
12	86.6	0.05	3.1	1.88
13	96.3	0.05	3.4	2.09
14	104.9	0.05	3.8	2.26
15	28.1	0.05	4.1	2.60
16	124.9	0.05	4.5	2.68
17	134.3	0.05	4.8	2.87
18	142.9	0.05	5.2	3.04
19	144.8	0.05	5.6	3.07
20	134.3	0.05	6.0	2.83
21	19.5	0.05	6.5	2.41
22	90.6	0.05	6.9	1.89

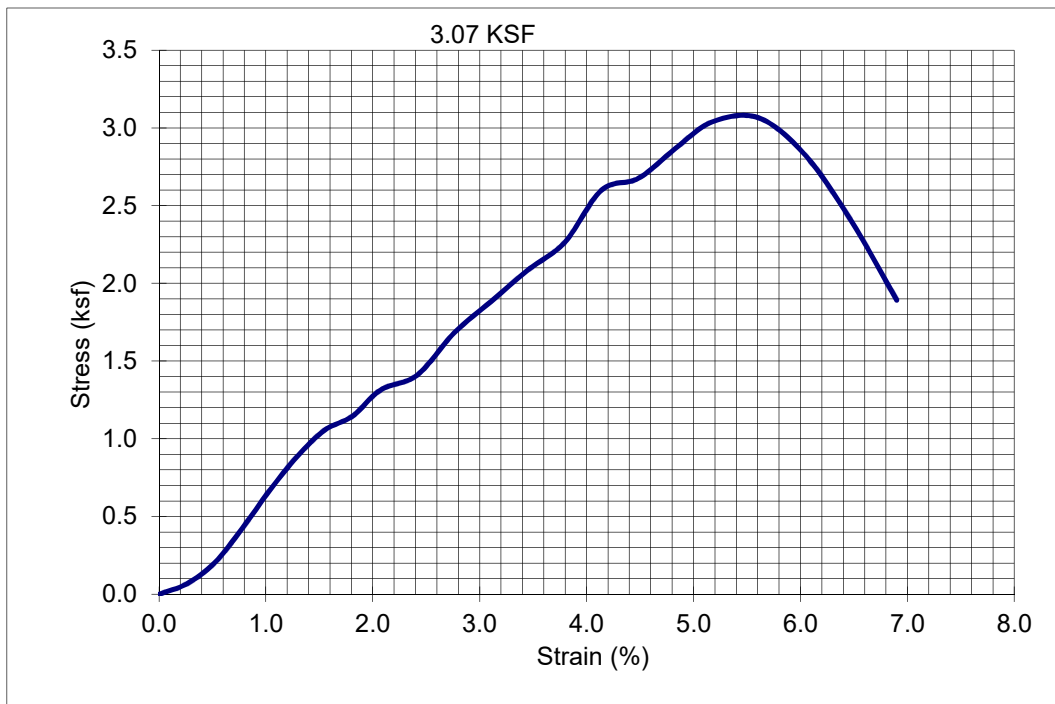


UNCONFINED COMPRESSION TEST

Project Name : Paducah Downtown Development	Sample # : ST-1
Project # : 10197216	Sample Loc. : Boring No. B-15
Project County : McCracken	Sample Depth : 19.5' to 20.0'
Project State : Kentucky	Date Tested : 11/20/2019
Laboratory # : 10197216	Date Reported : 11/21/2019
Submitted By : HDR	

Soil Type : Garth	Initial Height : 5.80 in
Wet Density : 130.4 pcf	Initial Diameter : 2.86 in
Dry Density : 110.6 pcf	Proving Ring : #22734
Moisture : 17.8 %	SPECIFIC GRAVITY : Garth
Deg. of Sat. : #VALUE! #VALUE!	

Comments : AASHTO: T-208



APPROVED BY: _____



UNCONFINED COMPRESSION TEST

AASHTO: T-208

Page 1 of 2

Project Name : Paducah Downtown Development
 Project # : 10197216
 Project County : McCracken
 Project State : Kentucky
 Laboratory # : 10197216
 Submitted By : HDR

Sample # : ST-1
 Sample Loc. : Boring No. B-8
 Sample Depth : 20.5' to 21.0'
 Date Tested : 11/19/2019
 Date Reported : 11/21/2019

Soil Type : Garth
 Wet Density : 132.9 pcf
 Dry Density : 114.1 pcf
 Moisture : 16.4 %

Initial Height : 5.84 in
 Initial Diameter : 2.85 in
 Proving Ring : #22734

RESULTS:	Axial Load	Corrected Area	Unit Strain	Stress
#	lbs	sf	%	Ksf
1	0.0	0.04	0.0	0.00
2	3.0	0.04	0.3	0.07
3	5.0	0.04	0.5	0.11
4	6.0	0.04	0.8	0.13
5	9.0	0.04	1.0	0.20
6	11.0	0.04	1.3	0.25
7	13.0	0.04	1.5	0.29
8	15.0	0.05	1.8	0.33
9	16.0	0.05	2.1	0.35
10	19.0	0.05	2.4	0.42
11	21.0	0.05	2.7	0.46
12	24.0	0.05	3.1	0.52
13	25.9	0.05	3.4	0.57
14	28.9	0.05	3.8	0.63
15	30.1	0.05	4.1	0.65
16	32.1	0.05	4.5	0.69
17	34.0	0.05	4.8	0.73
18	36.9	0.05	5.1	0.79
19	38.9	0.05	5.6	0.83
20	41.1	0.05	6.0	0.87
21	44.0	0.05	6.4	0.93
22	45.9	0.05	6.9	0.97
23	44.0	0.05	7.3	0.92
24	45.0	0.05	7.7	0.94
25	45.9	0.05	8.1	0.95
26	45.9	0.05	8.6	0.95
27	43.0	0.05	9.4	0.88
28	38.9	0.05	10.3	0.79

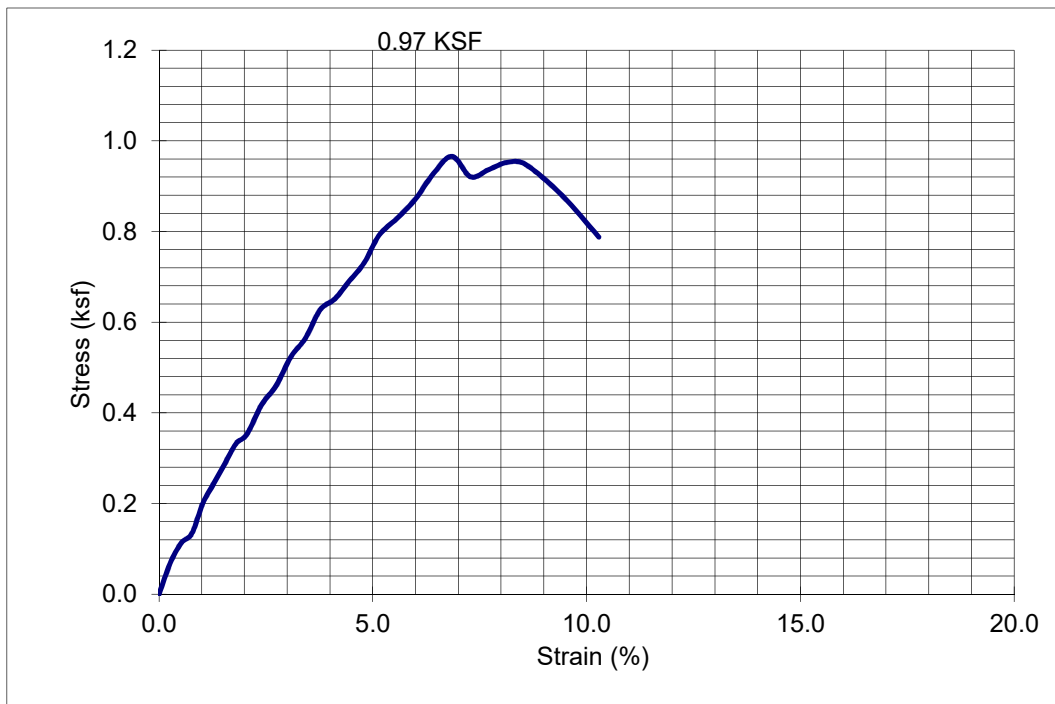


UNCONFINED COMPRESSION TEST

Project Name : Paducah Downtown Development	Sample # : ST-1
Project # : 10197216	Sample Loc. : Boring No. B-8
Project County : McCracken	Sample Depth : 20.5' to 21.0'
Project State : Kentucky	Date Tested : 11/19/2019
Laboratory # : 10197216	Date Reported : 11/21/2019
Submitted By : HDR	

Soil Type : Garth	Initial Height : 5.84 in
Wet Density : 132.9 pcf	Initial Diameter : 2.85 in
Dry Density : 114.1 pcf	Proving Ring : #22734
Moisture : 16.4 %	SPECIFIC GRAVITY : Garth
Deg. of Sat. : #VALUE! #VALUE!	

Comments : AASHTO: T-208



APPROVED BY: _____



UNCONFINED COMPRESSION TEST

AASHTO: T-208

Page 1 of 2

Project Name : Paducah Downtown Development	Sample # : ST-1
Project # : 10197216	Sample Loc. : Boring No. B-10
Project County : McCracken	Sample Depth : 20.0' to 20.5'
Project State : Kentucky	Date Tested : 11/19/2019
Laboratory # : 10197216	Date Reported : 11/21/2019
Submitted By : HDR	

Soil Type : Garth	Initial Height : 5.84 in
Wet Density : 132.6 pcf	Initial Diameter : 2.85 in
Dry Density : 111.4 pcf	Proving Ring : #22734
Moisture : 19.0 %	

RESULTS:	Axial Load	Corrected Area	Unit Strain	Stress
#	lbs	sf	%	Ksf
1	0.0	0.04	0.0	0.00
2	3.0	0.04	0.3	0.07
3	7.0	0.04	0.5	0.16
4	11.0	0.04	0.8	0.25
5	16.0	0.04	1.0	0.36
6	20.0	0.04	1.3	0.45
7	25.9	0.04	1.5	0.58
8	31.1	0.05	1.8	0.69
9	36.9	0.05	2.1	0.82
10	45.0	0.05	2.4	0.99
11	54.9	0.05	2.7	1.11
12	53.9	0.05	3.1	1.18
13	73.2	0.05	3.4	1.60
14	81.9	0.05	3.8	1.78
15	88.7	0.05	4.1	1.92
16	94.4	0.05	4.5	2.04
17	96.3	0.05	4.8	2.05
18	96.3	0.05	5.1	2.06
19	91.6	0.05	5.6	1.95
20	86.6	0.05	6.0	1.84

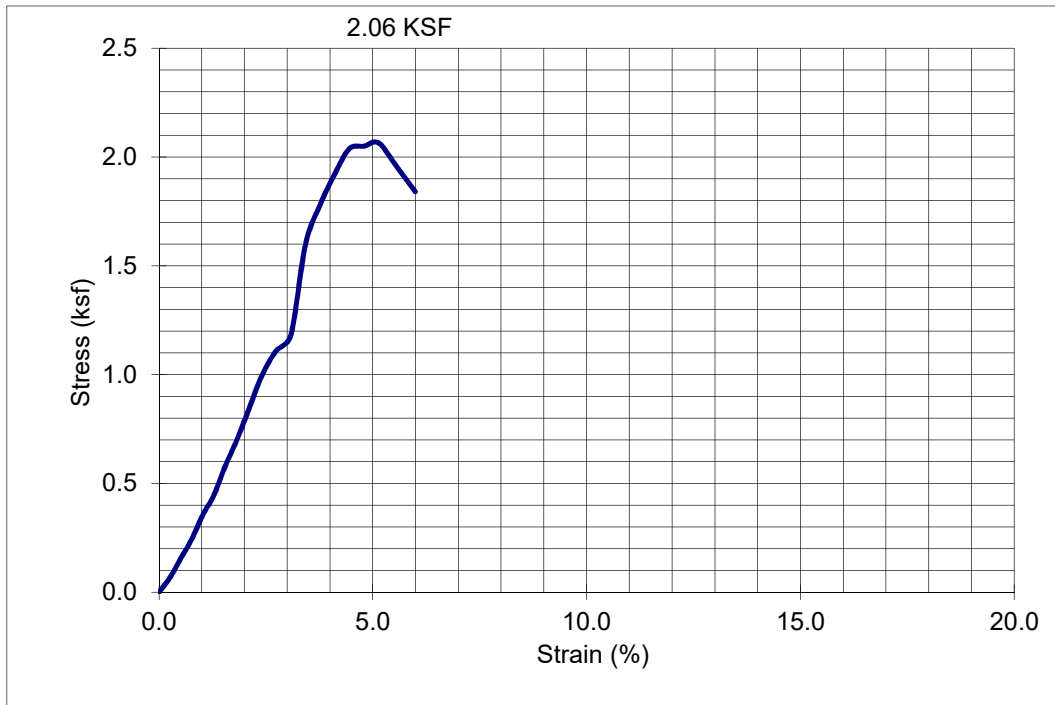


UNCONFINED COMPRESSION TEST

Project Name : Paducah Downtown Development	Sample # : ST-1
Project # : 10197216	Sample Loc. : Boring No. B-10
Project County : McCracken	Sample Depth : 20.0' to 20.5'
Project State : Kentucky	Date Tested : 11/19/2019
Laboratory # : 10197216	Date Reported : 11/21/2019
Submitted By : HDR	

Soil Type : Garth	Initial Height : 5.84 in
Wet Density : 132.6 pcf	Initial Diameter : 2.85 in
Dry Density : 111.4 pcf	Proving Ring : #22734
Moisture : 19.0 %	SPECIFIC GRAVITY : Garth
Deg. of Sat. : #VALUE! #VALUE!	

Comments : AASHTO: T-208



APPROVED BY: _____



UNCONFINED COMPRESSION TEST

AASHTO: T-208

Page 1 of 2

Project Name : Paducah Downtown Development	Sample # : ST-1
Project # : 10197216	Sample Loc. : Boring No. B-12
Project County : McCracken	Sample Depth : 20.0' to 20.5'
Project State : Kentucky	Date Tested : 11/19/2019
Laboratory # : 10197216	Date Reported : 11/21/2019
Submitted By : HDR	

Soil Type : Garth	Initial Height : 5.89 in
Wet Density : 130.7 pcf	Initial Diameter : 2.86 in
Dry Density : 110.1 pcf	Proving Ring : #22734
Moisture : 18.8 %	

RESULTS:	Axial Load	Corrected Area	Unit Strain	Stress
#	lbs	sf	%	Ksf
1	0.0	0.04	0.0	0.00
2	4.0	0.04	0.3	0.09
3	8.0	0.04	0.5	0.18
4	12.0	0.04	0.8	0.27
5	17.0	0.05	1.0	0.38
6	21.0	0.05	1.3	0.46
7	26.9	0.05	1.5	0.59
8	31.1	0.05	1.8	0.68
9	36.0	0.05	2.0	0.79
10	45.0	0.05	2.4	0.98
11	54.0	0.05	2.7	1.18
12	55.9	0.05	3.1	1.21
13	74.2	0.05	3.4	1.60
14	83.8	0.05	3.7	1.81
15	93.5	0.05	4.1	2.01
16	104.0	0.05	4.4	2.23
17	25.2	0.05	4.8	2.54
18	120.2	0.05	5.1	2.55
19	124.0	0.05	5.5	2.62
20	125.9	0.05	5.9	2.65
21	124.0	0.05	6.4	2.60
22	120.2	0.05	6.8	2.51
23	31.0	0.05	7.2	1.64

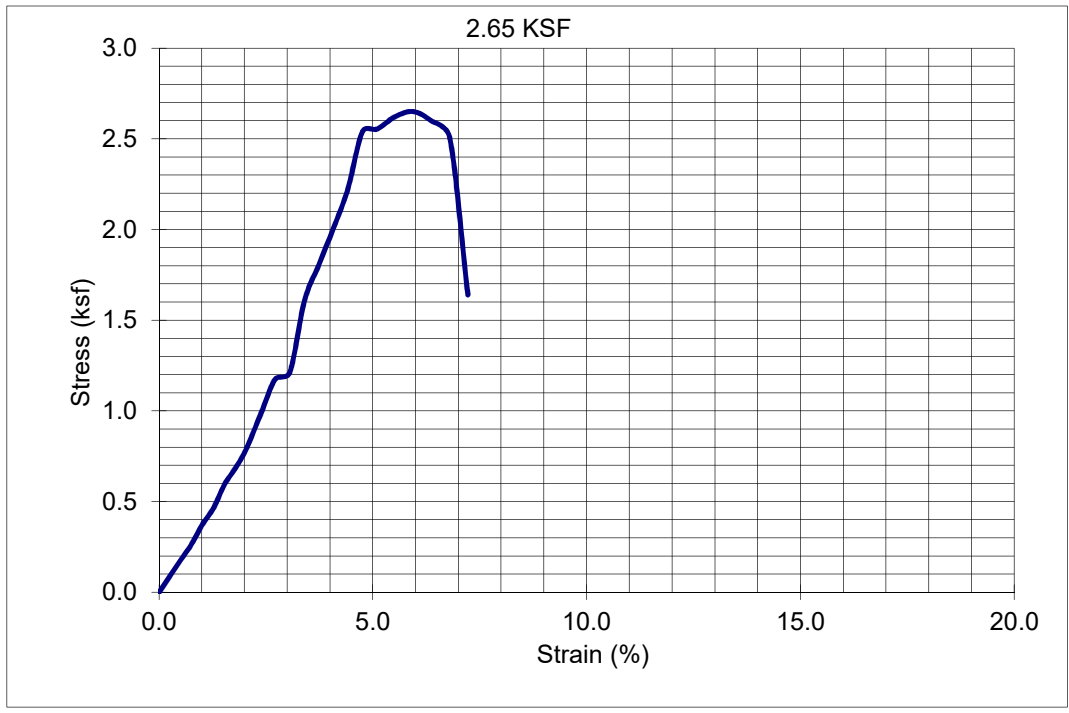


UNCONFINED COMPRESSION TEST

Project Name : Paducah Downtown Development	Sample # : ST-1
Project # : 10197216	Sample Loc. : Boring No. B-12
Project County : McCracken	Sample Depth : 20.0' to 20.5'
Project State : Kentucky	Date Tested : 11/19/2019
Laboratory # : 10197216	Date Reported : 11/21/2019
Submitted By : HDR	

Soil Type : Garth	Initial Height : 5.89 in
Wet Density : 130.7 pcf	Initial Diameter : 2.86 in
Dry Density : 110.1 pcf	Proving Ring : #22734
Moisture : 18.8 %	SPECIFIC GRAVITY : Garth
Deg. of Sat. : #VALUE! #VALUE!	

Comments : AASHTO: T-208



APPROVED BY: _____



UNCONFINED COMPRESSION TEST

AASHTO: T-208

Page 1 of 2

Project Name : Paducah Downtown Development	Sample # : ST-1
Project # : 10197216	Sample Loc. : Boring No. B-13
Project County : McCracken	Sample Depth : 20.0' to 20.5'
Project State : Kentucky	Date Tested : 11/20/2019
Laboratory # : 10197216	Date Reported : 11/21/2019
Submitted By : HDR	

Soil Type : Garth	Initial Height : 5.81 in
Wet Density : 129.5 pcf	Initial Diameter : 2.85 in
Dry Density : 109.7 pcf	Proving Ring : #22734
Moisture : 18.1 %	

RESULTS:	Axial Load	Corrected Area	Unit Strain	Stress
#	lbs	sf	%	Ksf
1	0.0	0.04	0.0	0.00
2	4.0	0.04	0.3	0.09
3	9.0	0.04	0.5	0.20
4	14.0	0.04	0.8	0.31
5	19.0	0.04	1.0	0.42
6	23.0	0.04	1.3	0.51
7	27.9	0.05	1.5	0.62
8	35.0	0.05	1.8	0.77
9	40.1	0.05	2.1	0.88
10	45.0	0.05	2.4	0.99
11	51.1	0.05	2.8	1.12
12	54.0	0.05	3.1	1.18
13	57.8	0.05	3.4	1.26
14	58.8	0.05	3.8	1.27
15	59.8	0.05	4.1	1.29
16	55.9	0.05	4.5	1.20
17	48.8	0.05	4.8	1.05
18	43.0	0.05	5.2	0.92

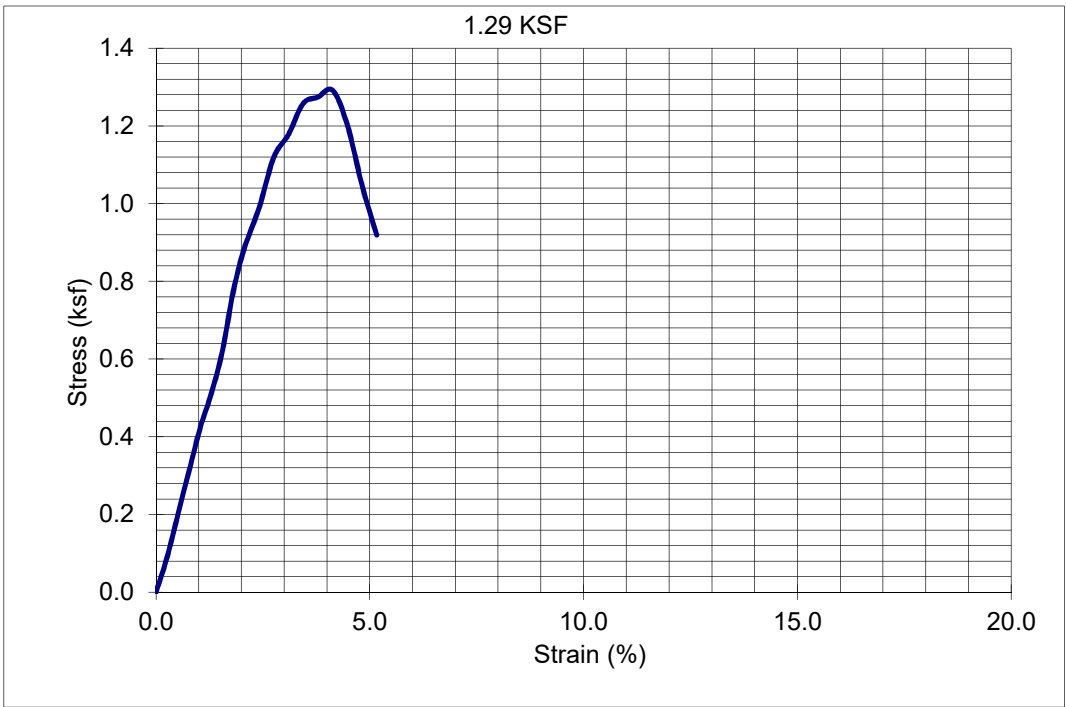


UNCONFINED COMPRESSION TEST

Project Name : Paducah Downtown Development	Sample # : ST-1
Project # : 10197216	Sample Loc. : Boring No. B-13
Project County : McCracken	Sample Depth : 20.0' to 20.5'
Project State : Kentucky	Date Tested : 11/20/2019
Laboratory # : 10197216	Date Reported : 11/21/2019
Submitted By : HDR	

Soil Type : Garth	Initial Height : 5.81 in
Wet Density : 129.5 pcf	Initial Diameter : 2.85 in
Dry Density : 109.7 pcf	Proving Ring : #22734
Moisture : 18.1 %	SPECIFIC GRAVITY : Garth
Deg. of Sat. : #VALUE! #VALUE!	

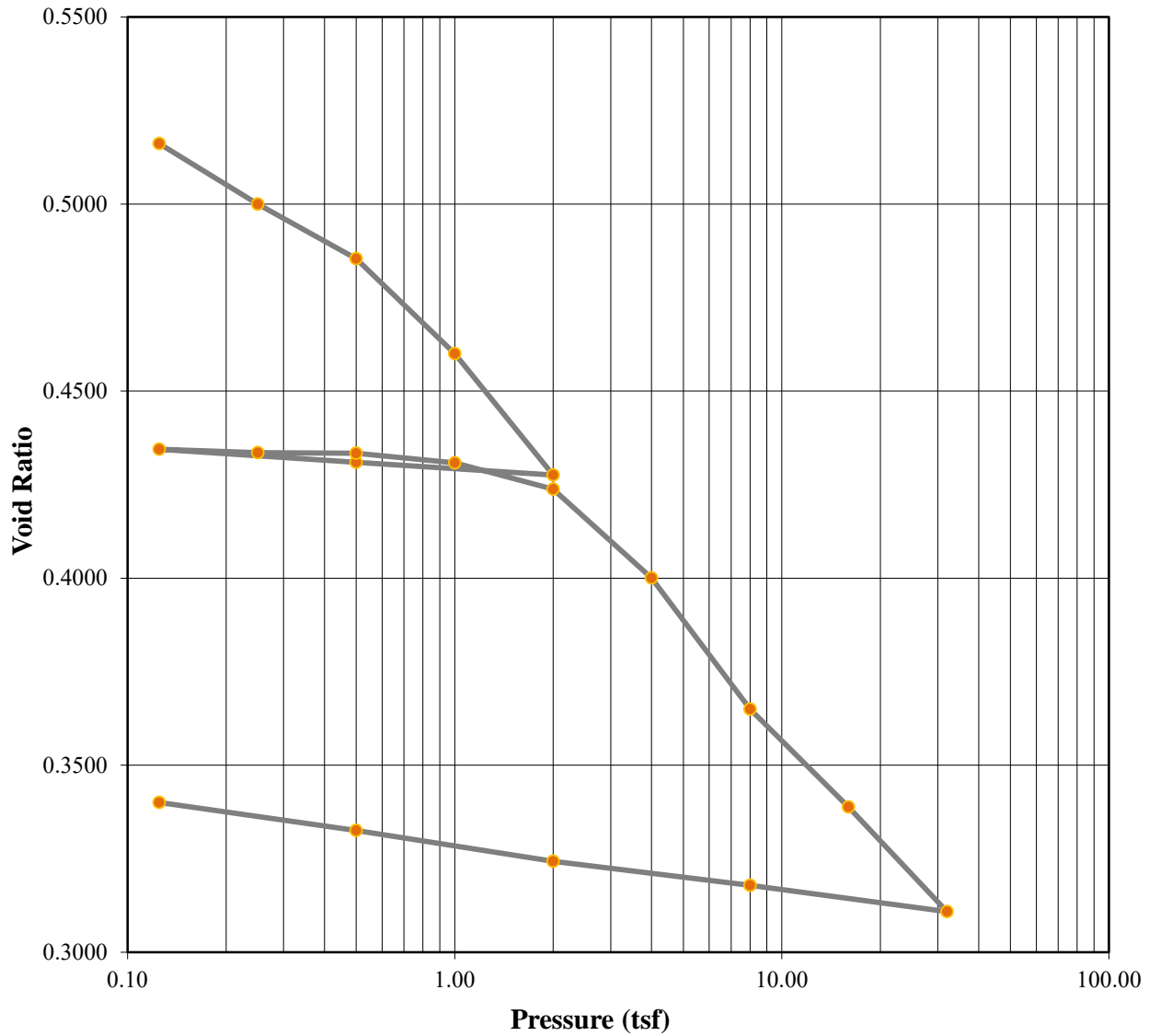
Comments : AASHTO: T-208



APPROVED BY: _____



CONSOLIDATION TEST



Summary of Consolidation Test Results				Test Date:	
Overburden Press. (tsf)	0.60	Compression Index, C_c	0.10		
Preconsol. Press., P_c (tsf)	0.60		Rebound Index, C_r	0.01	
Over Consolidation Ratio	1.00				
Soil Description	Brown Lean Clay with Sand				
Project Number:	10197216	Depth: 20.3' to 20.5'	Remarks: ASTM D2435/D2435M-11		
Sample Number:	ST-1	Boring Number: B-8			
Project:	Paducah City Block Development				
Client:					
Location:	McCracken Co., Kentucky				



TRANSMITTAL LETTER

DATE: December 3, 2019

ATTENTION: Kevin Walker

TO: HDR, Paducah
4645 Village Square Drive, Suite F
Paducah, KY 42001

SUBJECT: Laboratory Test Data
Paducah City Block Development
Your #10197216, HDR Lab #19-0844LAB

COMMENTS: Enclosed are the results for the subject project.

A handwritten signature in black ink, appearing to read 'James T. Keegan', written over a horizontal line.

James T. Keegan, MD
Corrosion and Lab Services Section Manager



Table 1 - Laboratory Tests on Soil Samples

HDR, Paducah
Paducah City Block Development
Your #10197216, HDR Lab #19-0844LAB
3-Dec-19

Sample ID		B-1 @ 9- 20.5'	B-3 @ 14- 25.5'	B-8 @ 28.3- 9.8'	B-10 @ 24- 35.5'
Resistivity					
as-received	ohm-cm	>4,400,000	>4,400,000	>4,400,000	>4,400,000
saturated	ohm-cm	2,720	5,200	7,600	8,400
pH					
		7.3	3.9	5.9	6.1
Electrical					
Conductivity	mS/cm	na	na	na	na
Chemical Analyses					
Cations					
calcium	Ca ²⁺ mg/kg	na	na	na	na
magnesium	Mg ²⁺ mg/kg	na	na	na	na
sodium	Na ¹⁺ mg/kg	na	na	na	na
potassium	K ¹⁺ mg/kg	na	na	na	na
Anions					
carbonate	CO ₃ ²⁻ mg/kg	na	na	na	na
bicarbonate	HCO ₃ ¹⁻ mg/kg	na	na	na	na
fluoride	F ¹⁻ mg/kg	na	na	na	na
chloride	Cl ¹⁻ mg/kg	na	na	na	na
sulfate	SO ₄ ²⁻ mg/kg	na	na	na	na
phosphate	PO ₄ ³⁻ mg/kg	na	na	na	na
Other Tests					
ammonium	NH ₄ ¹⁺ mg/kg	na	na	na	na
nitrate	NO ₃ ¹⁻ mg/kg	na	na	na	na
sulfide	S ²⁻ qual	na	na	na	na
Redox	mV	na	na	na	na

Resistivity per ASTM G187, Cations per ASTM D6919, Anions per ASTM D4327, and Alkalinity per APHA 2320-B.

Electrical conductivity in millisiemens/cm and chemical analyses were made on a 1:5 soil-to-water extract.

mg/kg = milligrams per kilogram (parts per million) of dry soil.

Redox = oxidation-reduction potential in millivolts

ND = not detected

na = not analyzed

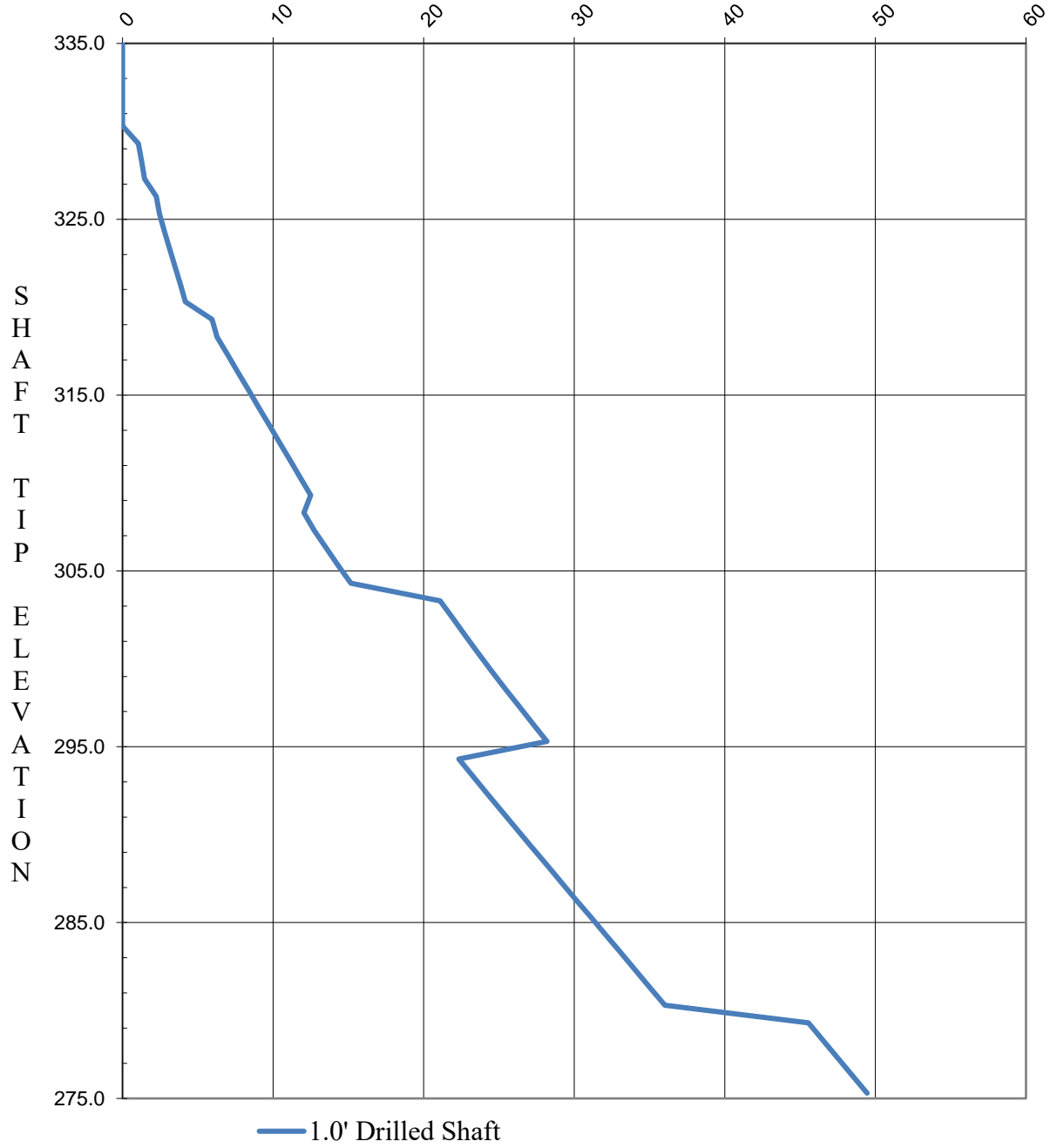
Appendix D: Calculations



ALLOWABLE SHAFT CAPACITY CURVE Paducah City Block Development-Hotel

Factor of Safety = 2.5

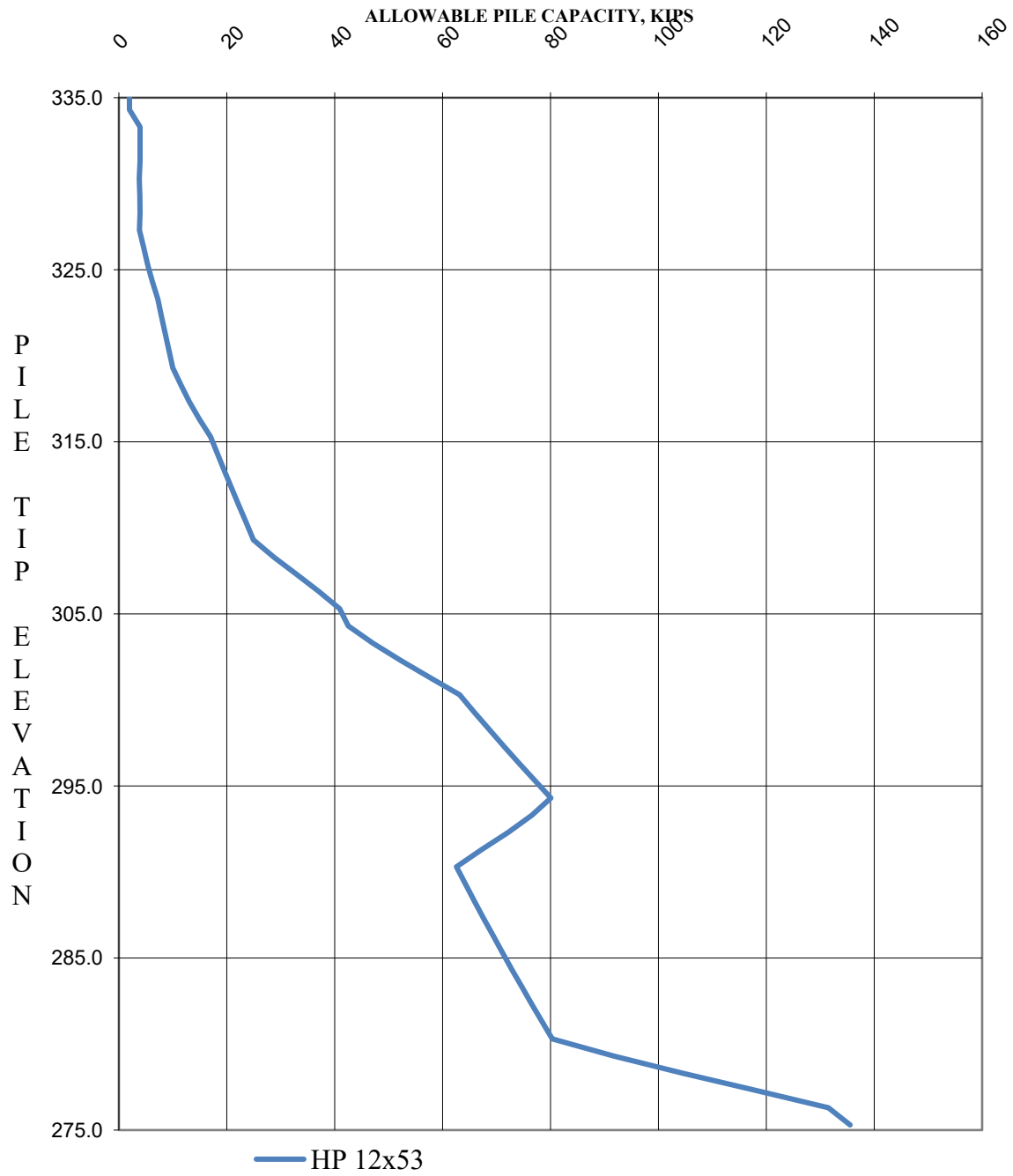
ALLOWABLE SHAFT CAPACITY, TON





Allowable Pile Capacity Curve Paducah City Block Development-Hotel

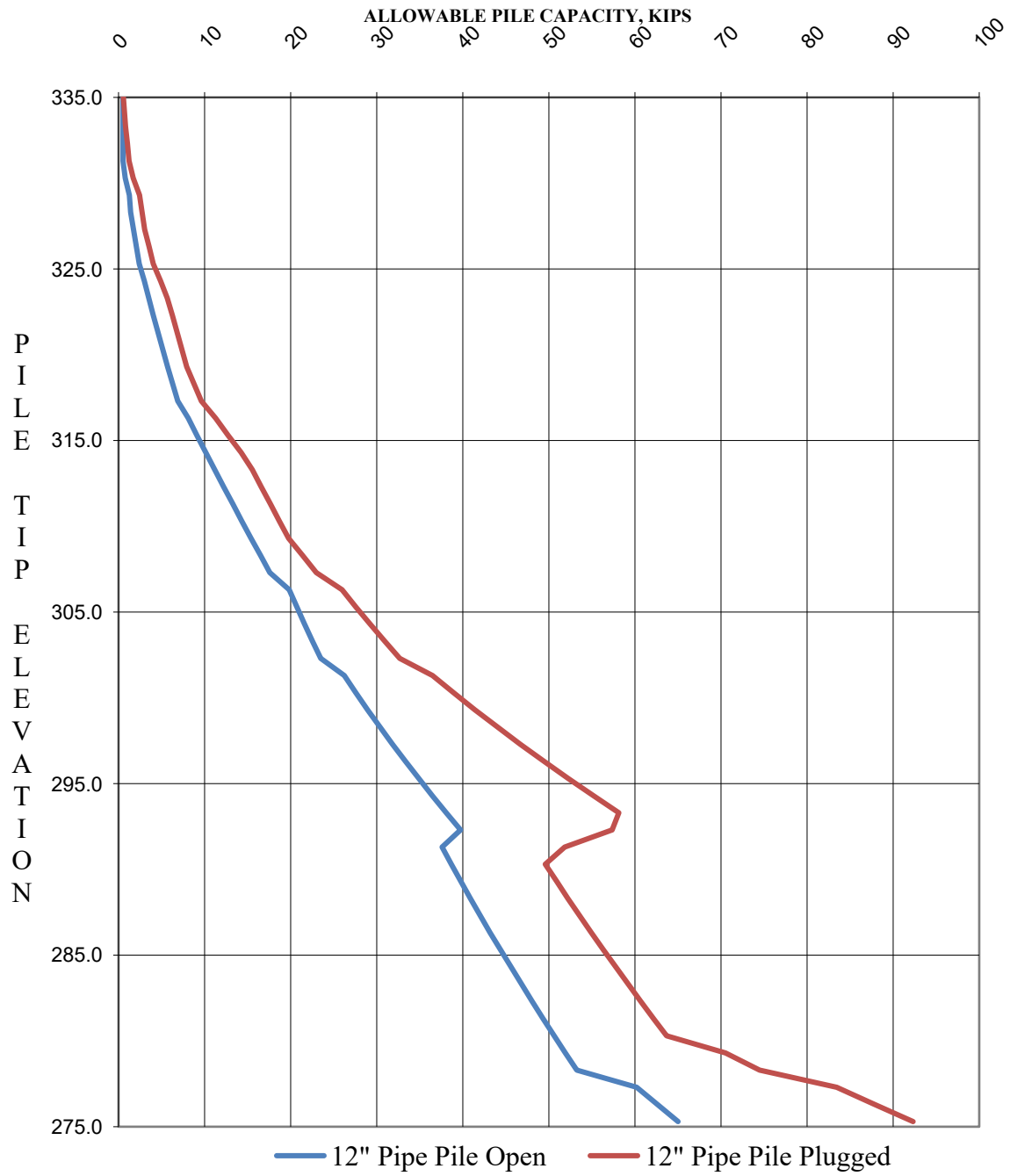
Factor of Safety = 2.75





Allowable Pile Capacity Curve Paducah City Block Development-Hotel

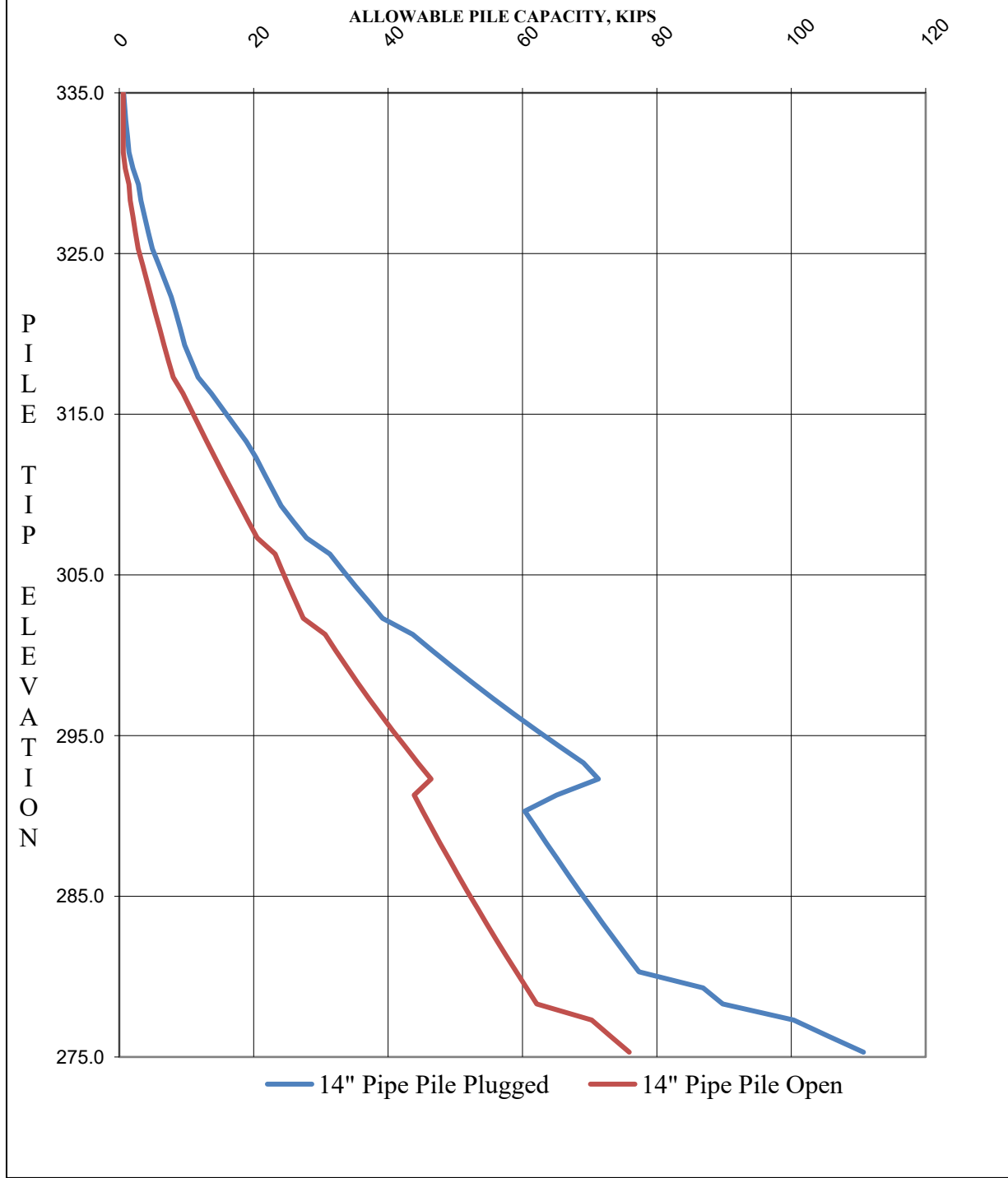
Factor of Safety = 2.75





Allowable Pile Capacity Curve Paducah City Block Development-Hotel

Factor of Safety = 2.75

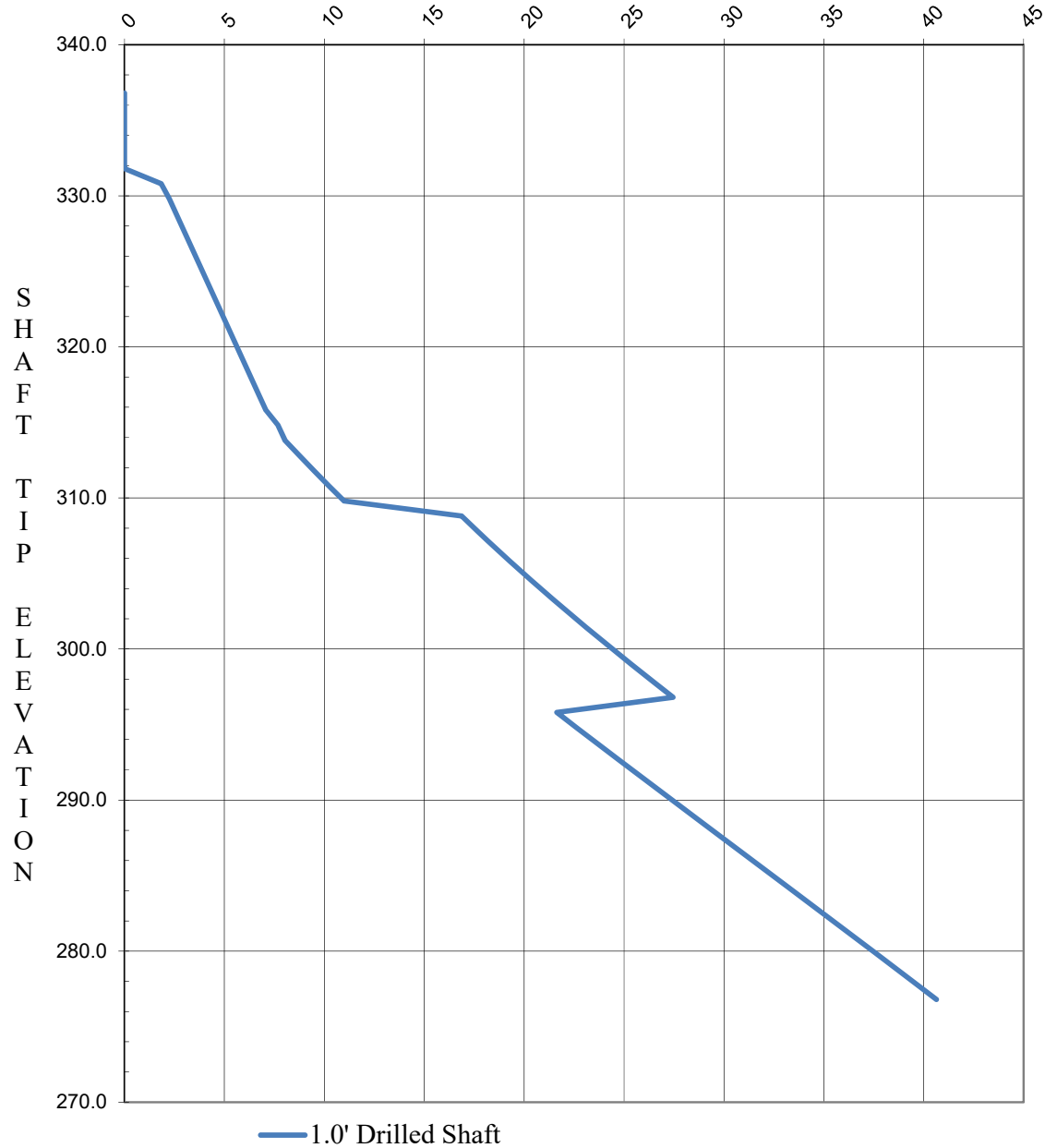




ALLOWABLE SHAFT CAPACITY CURVE Paducah City Block Development-Mixed Use Buildings

Factor of Safety = 2.5

ALLOWABLE SHAFT CAPACITY, TON

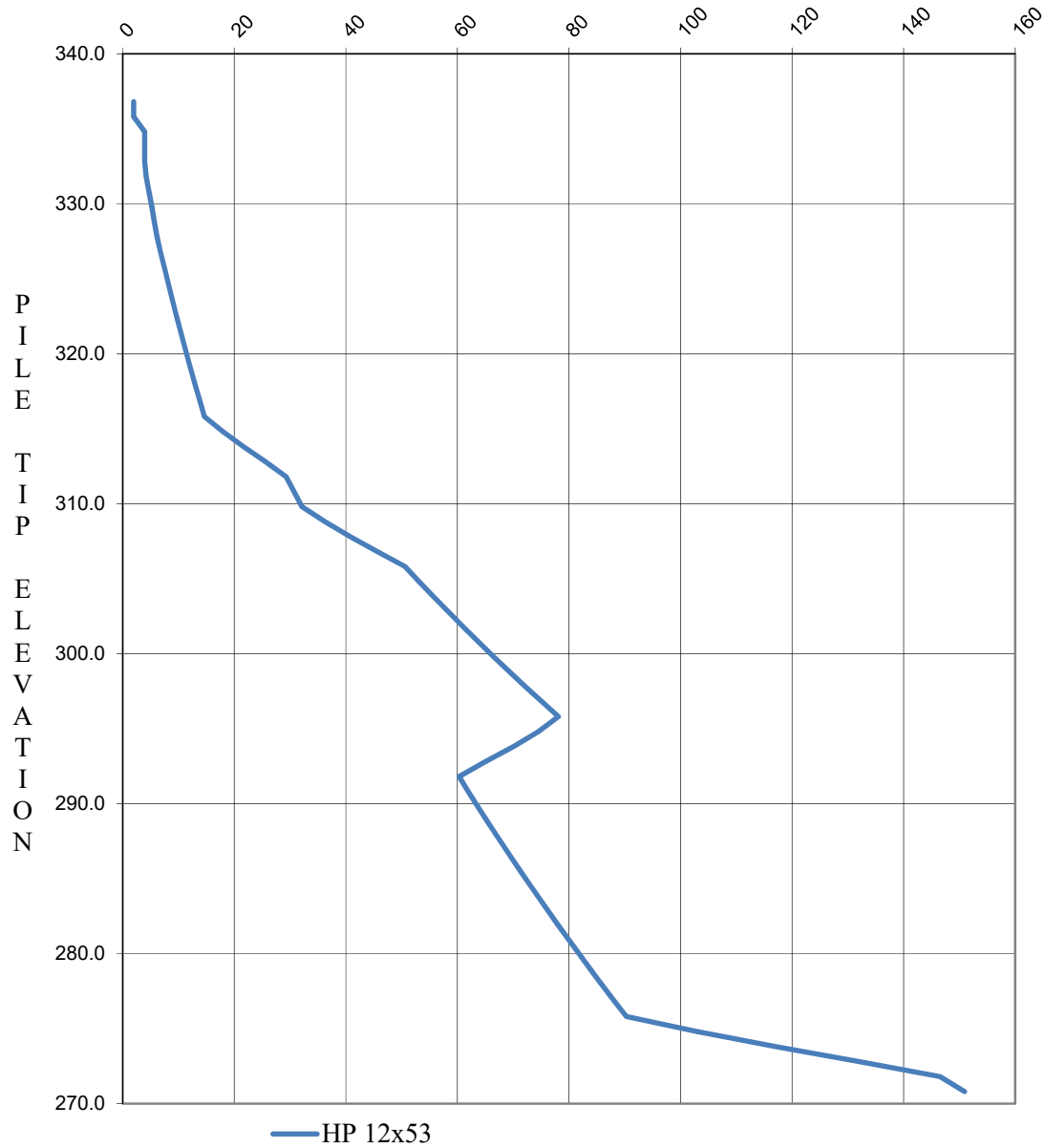




Allowable Pile Capacity Curve Paducah City Block Development-Mixed Use Buildings

Factor of Safety = 2.75

ALLOWABLE PILE CAPACITY, KIPS

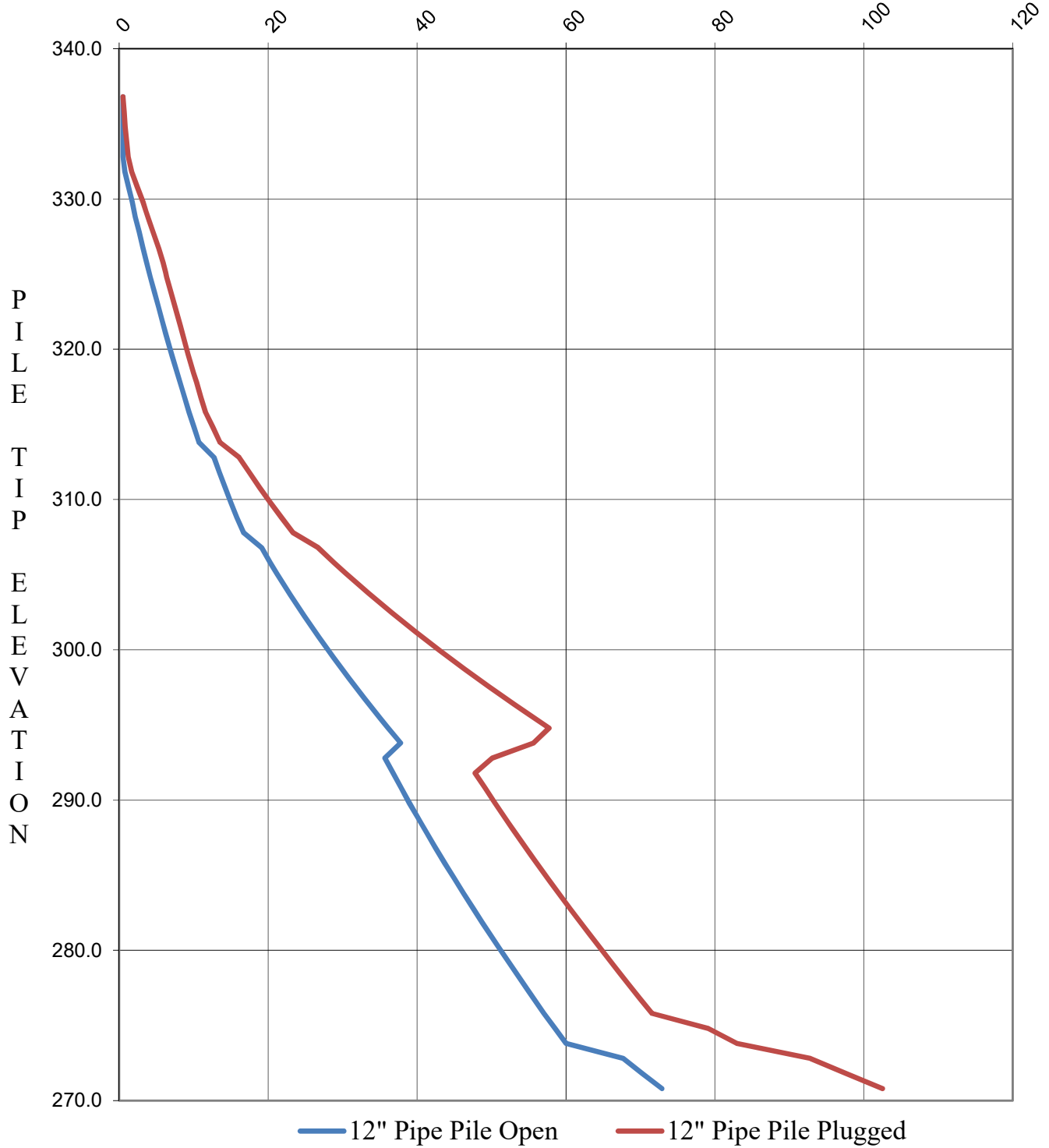


Allowable Pile Capacity Curve

Paducah City Block Development-Mixed Use Buildings

Factor of Safety = 2.75

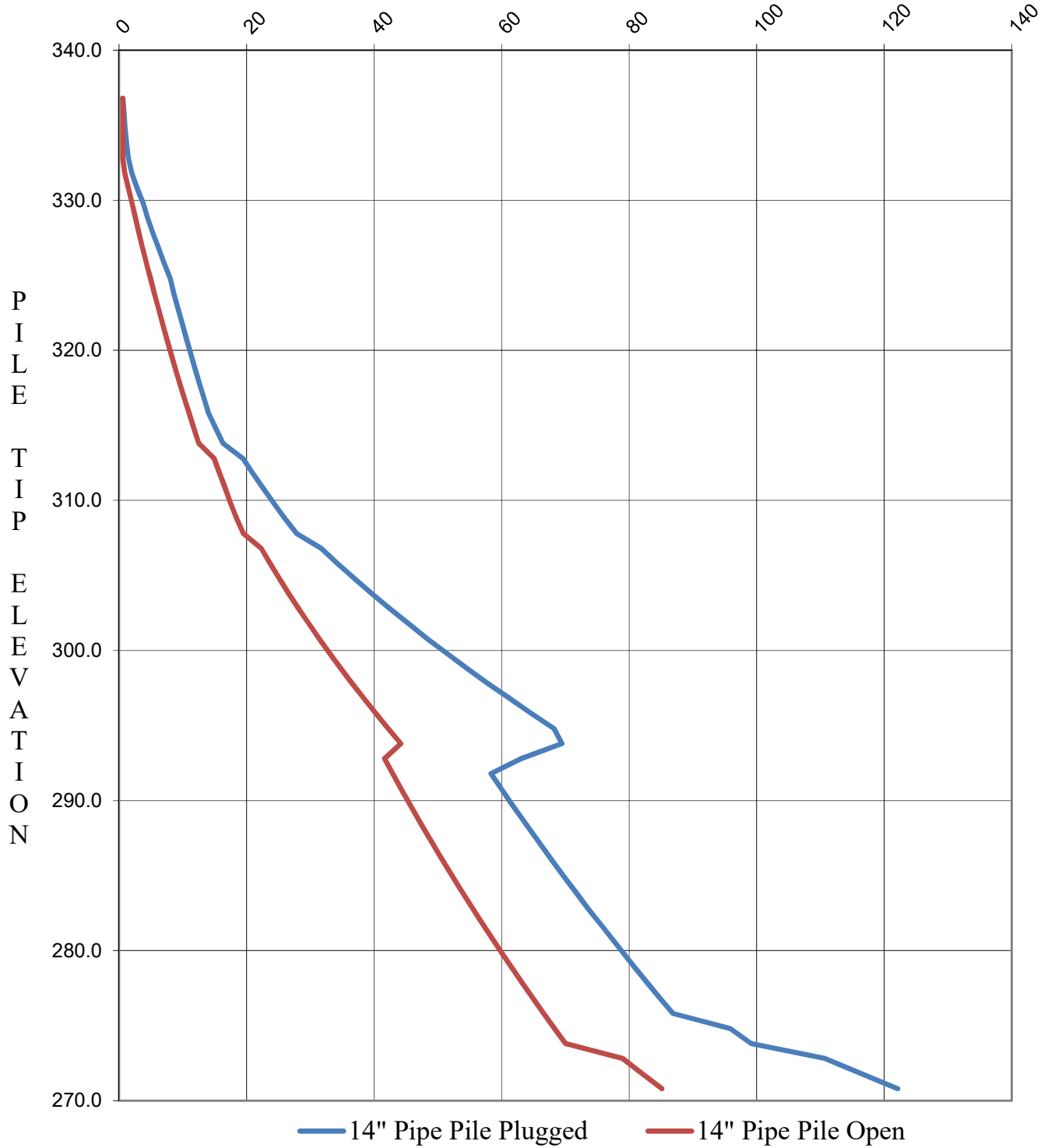
ALLOWABLE PILE CAPACITY, KIPS

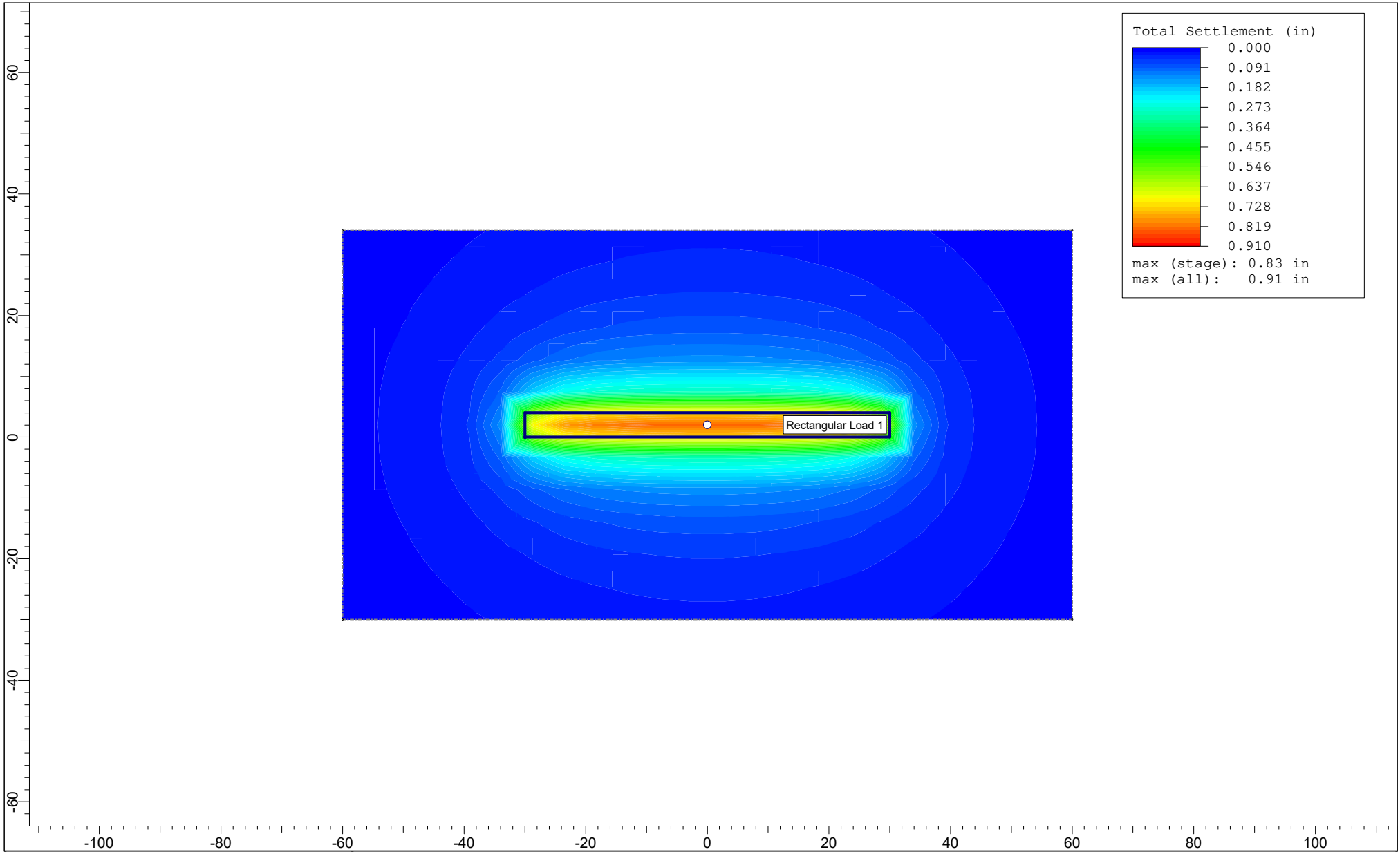


Allowable Pile Capacity Curve Paducah City Block Development-Mixed Use Buildings

Factor of Safety = 2.75

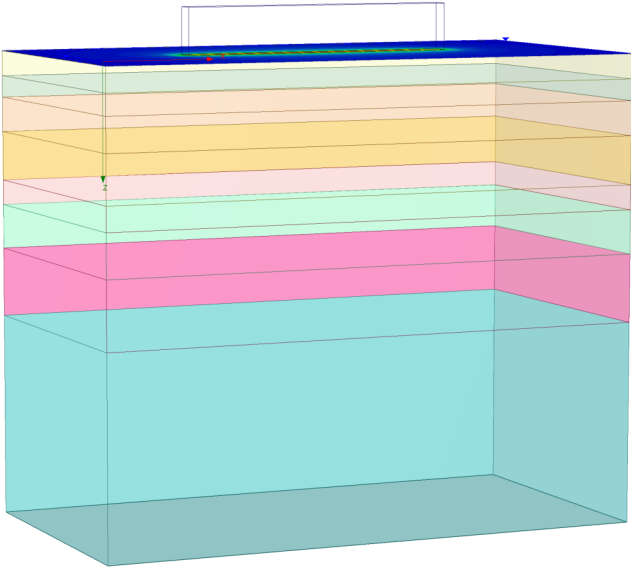
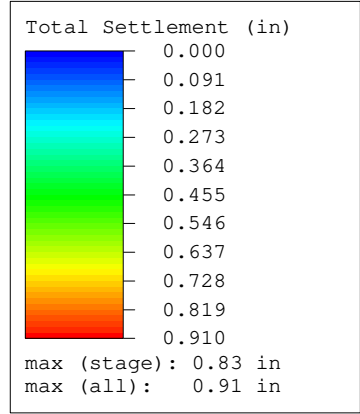
ALLOWABLE PILE CAPACITY, KIPS





SETTLE3D 4.006

<i>Project</i>	City of Paducah		
<i>Analysis Description</i>	Settlement with 1500 PSF Load		
<i>Drawn By</i>	JRH	<i>Company</i>	HDR
<i>Date</i>	12/10/2019, 2:10:42 PM	<i>File Name</i>	Paducah1500PSF.s3z



SETTLE3D 4.006

<i>Project</i>	City of Paducah		
<i>Analysis Description</i>	Settlement with 1500 PSF Load		
<i>Drawn By</i>	JRH	<i>Company</i>	HDR
<i>Date</i>	12/10/2019, 2:10:42 PM	<i>File Name</i>	Paducah1500PSF.s3z

Settle3D Analysis Information

City of Paducah

Project Settings

Document Name	Paducah1500PSF.s3z
Project Title	City of Paducah
Analysis	Settlement with 1500 PSF Load
Author	JRH
Company	HDR
Date Created	12/10/2019, 2:10:42 PM
Stress Computation Method	Boussinesq
Time-dependent Consolidation Analysis	
Time Units	days
Permeability Units	feet/day
Minimum settlement ratio for subgrade modulus	0.9

Use average properties to calculate layered stresses

Improve consolidation accuracy

Ignore negative effective stresses in settlement calculations

Stage Settings

Stage #	Name	Time [days]
1	Stage 1	0
2	Stage 2	230
3	Stage 3	100000

Results

Time taken to compute: 0 seconds

Stage: Stage 1 = 0 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.0561033
Total Consolidation Settlement [in]	0	0
Virgin Consolidation Settlement [in]	0	0
Recompression Consolidation Settlement [in]	0	0
Immediate Settlement [in]	0	0.0561033
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0	1.5
Loading Stress XX [ksf]	-0.126399	0.894201
Loading Stress YY [ksf]	-0.0638043	1.46157
Effective Stress ZZ [ksf]	0	6.1845
Effective Stress XX [ksf]	-0.126399	2.22718
Effective Stress YY [ksf]	-0.0638043	2.22795
Total Stress ZZ [ksf]	0	12.4405
Total Stress XX [ksf]	-0.126399	8.48083
Total Stress YY [ksf]	-0.0638043	8.48373
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	468.163
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	468.163
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	0
Total Strain	0	0.000194994
Pore Water Pressure [ksf]	0	6.25598
Excess Pore Water Pressure [ksf]	0	1.5
Degree of Consolidation [%]	0	0
Pre-consolidation Stress [ksf]	1.6234	6.18159
Over-consolidation Ratio	1	157.233
Void Ratio	0	0.562
Permeability [ft/d]	0	0.0043195
Coefficient of Consolidation [ft ² /d]	0	0.376
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	1.2369

Stage: Stage 2 = 230 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.828691
Total Consolidation Settlement [in]	0	0.772588
Virgin Consolidation Settlement [in]	0	0
Recompression Consolidation Settlement [in]	0	0.772588
Immediate Settlement [in]	0	0.0561033
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0	1.5
Loading Stress XX [ksf]	-0.126399	0.894201
Loading Stress YY [ksf]	-0.0638043	1.46157
Effective Stress ZZ [ksf]	0	6.20048
Effective Stress XX [ksf]	-0.126399	2.3942
Effective Stress YY [ksf]	-0.0638043	2.96157
Total Stress ZZ [ksf]	0	12.4405
Total Stress XX [ksf]	-0.126399	8.48083
Total Stress YY [ksf]	-0.0638043	8.48373
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	25.9641
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	468.163
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	27.4886
Total Strain	-3.42045e-006	0.0166054
Pore Water Pressure [ksf]	0	6.24
Excess Pore Water Pressure [ksf]	0	0.124473
Degree of Consolidation [%]	0	99.8637
Pre-consolidation Stress [ksf]	1.62624	6.19759
Over-consolidation Ratio	1	157.367
Void Ratio	0	0.562005
Permeability [ft/d]	0	0.0043195
Coefficient of Consolidation [ft ² /d]	0	0.376
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	1.23754

Stage: Stage 3 = 100000 d

Data Type	Minimum	Maximum
Total Settlement [in]	0	0.906579
Total Consolidation Settlement [in]	0	0.850475
Virgin Consolidation Settlement [in]	0	0
Recompression Consolidation Settlement [in]	0	0.850475
Immediate Settlement [in]	0	0.0561033
Secondary Settlement [in]	0	0
Loading Stress ZZ [ksf]	0	1.5
Loading Stress XX [ksf]	-0.126399	0.894201
Loading Stress YY [ksf]	-0.0638043	1.46157
Effective Stress ZZ [ksf]	0	6.20048
Effective Stress XX [ksf]	-0.126399	2.3942
Effective Stress YY [ksf]	-0.0638043	2.96157
Total Stress ZZ [ksf]	0	12.4405
Total Stress XX [ksf]	-0.126399	8.48083
Total Stress YY [ksf]	-0.0638043	8.48373
Modulus of Subgrade Reaction (Total) [ksf/ft]	0	24.024
Modulus of Subgrade Reaction (Immediate) [ksf/ft]	0	468.163
Modulus of Subgrade Reaction (Consolidation) [ksf/ft]	0	25.3235
Total Strain	2.39488e-009	0.0166058
Pore Water Pressure [ksf]	0	6.24
Excess Pore Water Pressure [ksf]	-4.49296e-018	9.81696e-018
Degree of Consolidation [%]	0	100
Pre-consolidation Stress [ksf]	1.62624	6.19759
Over-consolidation Ratio	1	157.233
Void Ratio	0	0.562
Permeability [ft/d]	0	0.0043195
Coefficient of Consolidation [ft ² /d]	0	0.376
Hydroconsolidation Settlement [in]	0	0
Average Degree of Consolidation [%]	0	0
Undrained Shear Strength	0	1.23754

Loads

1. Rectangular Load: "Rectangular Load 1"

Length 60 ft
 Width 4 ft
 Rotation angle 0 degrees
 Load Type Flexible
 Area of Load 240 ft²
 Load 1.5 ksf
 Depth 0 ft
 Installation Stage Stage 1 = 0 d

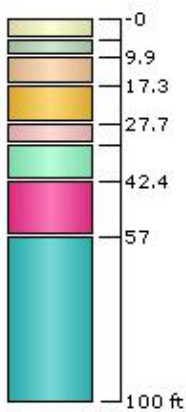
Coordinates

X [ft]	Y [ft]
-30	0
30	0
30	4
-30	4





Soil Layers





Ground Surface Drained: Yes

Layer #	Type	Thickness [ft]	Depth [ft]	Drained at Bottom
1	Lean Clay	5.3	0	No
2	Silty Clay I	4.6	5.3	No
3	Silty Clay II	7.4	9.9	No
4	Silty Clay III	10.4	17.3	Yes
5	Poorly-Graded Gravel I	5.3	27.7	No
6	Poorly-Graded Gravel II	9.4	33	No
7	Poorly-Graded Gravel and Silty Sand	14.6	42.4	No
8	Silty Sand	43	57	No



Soil Properties

Property	Lean Clay	Silty Clay I	Silty Clay II	Silty Clay III
Color				
Unit Weight [kips/ft ³]	0.12	0.12	0.12	0.12
Saturated Unit Weight [kips/ft ³]	0.12	0.12	0.12	0.12
K0	1	1	1	1
Primary Consolidation	Enabled	Enabled	Enabled	Enabled
Material Type	Non-Linear	Non-Linear	Non-Linear	Non-Linear
Cc	0.12	0.12	0.12	0.12
Cr	0.013	0.013	0.013	0.013
e0	0.562	0.562	0.562	0.562
Pc [ksf]	2.4	2.4	2.4	2.4
Cv [ft ² /d]	0.292	0.292	0.376	0.376
Cvr [ft ² /d]	0.292	0.292	0.376	0.376
B-bar	1	1	1	1
Undrained Su A [kips/ft ²]	0	0	0	0
Undrained Su S	0.2	0.2	0.2	0.2
Undrained Su m	0.8	0.8	0.8	0.8
Piezo Line ID	1	1	1	1

Property	Poorly-Graded Gravel I	Poorly-Graded Gravel II	Poorly-Graded Gravel and Silty Sand	Silty Sand
Color				
Unit Weight [kips/ft ³]	0.115	0.13	0.115	0.13
Saturated Unit Weight [kips/ft ³]	0.115	0.13	0.115	0.13
K0	0.47	0.38	0.53	0.36
Immediate Settlement	Enabled	Enabled	Enabled	Enabled
Es [ksf]	800	1500	350	1000
Esur [ksf]	800	1500	350	1000
B-bar	-	-	-	-
Undrained Su A [kips/ft ²]	0	0	0	0
Undrained Su S	0.2	0.2	0.2	0.2
Undrained Su m	0.8	0.8	0.8	0.8
Piezo Line ID	1	1	1	1

Groundwater

Groundwater method Piezometric Lines
 Water Unit Weight 0.0624 kips/ft³

Piezometric Line Entities

ID	Depth (ft)
1	0 ft

Field Point Grid

Number of points 342
 Expansion Factor 2

Grid Coordinates

X [ft]	Y [ft]
60	34
60	-30
-60	-30
-60	34

Time Points

Point #	(X,Y) Location	Depth	Goal Type	Goal	Time Until Goal
1	0, 2	0 ft	Degree of Consolidation	90%	0 d